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SINGLE-STAGE EVALUATION OF HIGHLY-LOADED HIGH-MACH-NUMBER COMPRESSOR STAGES VI. DATA AND PERFORMANCE OF CANTILEVERED STATOR

By

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PRATT & WHITNEY AIRCRAFT DIVISION UNITED AIRCRAFT CORPORATION

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FOREWORD

This report was prepared by the Pratt & Whitney Aircraft Division of United Aircraft Corporation, East Hartford, Connecticut, to present data and performance of a compressor stage with a cantilevered stator and a rotating inner shroud beneath the stator.

TABLE OF CONTENTS

		Page
I	SUMMARY	1
П	INTRODUCTION	2
III	APPARATUS AND PROCEDURE	2
	A. Test Compressor B. Instrumentation and Calibration C. Test Procedure D. Calculation Procedure	2 2 6 6
IV	RESULTS AND DISCUSSION	7
	 A. Overall Performance B. Stator Exit Gapwise Distribution of Total Pressure C. Blade Element Performance D. Controur Plots of Stator Exit Survey Data E. Rapid Response Hot-Film Data 	7 8 8 9
V	SUMMARY REMARKS	9
Ref	erences	10
App	pendix 1 Performance Parameters	61
App	pendix 2 Symbols	64
App	pendix 3 Overall and Blade Element Performance	67

LIST OF FIGURES

Figure	Title	Page
1	Cross Section of Test Compressor	11
2	Cantilevered Stator and Rotating Shroud Assembly	12
3	Axial Station Number Designation and Location of Instrumentation	13
4.	Circumferential Location of Instrumentation, Viewed From Rear	14
5	Photographs of Typical Instrumentation	15
6	Rotor Overall Performance Comparison, Cantilevered Versus Shrouded Stator	16
7	Stage Overall Performance Comparison, Cantilevered Versus Shrouded Stator	17
8	Comparison of Stage Spanwise Performance, Cantilevered Versus Shrouded Stator, Tangential Probe Data, 100 Percent of Design Speed	18
9	Stator Exit Gapwise Total Pressure Distribution Cantilevered Versus Shrouded Stator Near Stall Flow Condition, 100 Percent Design Speed	19
10	Stator Exit Gapwise Total Pressure Distribution Cantilevered Versus Shrouded Stator Design Flow Condition, 100 Percent Design Speed	20
11	Stator Exit Gapwise Total Pressure Distribution Cantilevered Versus Shrouded Stator Wide Open Throttle Condition, 100 Percent Design Speed	21
12	Rotor Blade Element Performance	22-30
13	Stator Blade Element Performance	31-39
14	Rotor Blade Element Performance Comparison Cantilevered Versus Shrouded at 100 Percent Design Speed	40-44

LIST OF FIGURES (Cont'd)

Figure	Title	Page
15	Stator Blade Element Performance Comparison Cantilevered Versus Shrouded at 100 Percent Design Speed	45-49
16	Total Pressure Ratio, Stator Exit Contour Plots	50-51
. 17	Total Temperature Ratio, Stator Exit Contour Plots	52-53
18	Stator Exit Absolute Air Angle, Stator Exit Contour Plots	54-55
19	Static Pressure Ratio, Stator Exit Contour Plots	56-57
20	Meridional Velocity, Stator Exit Contour Plots	58-59
21	Oscillograph Trace of Typical Surge Cycle at 100 Percent Design Speed	60

LIST OF TABLES

Number	Title	Page
1	MCA Rotor and Stator Design Parameters	3
2	Performance and Blade Element Instrumentation	4
3	Stall Instrumentation	5
. 4	Identification of Blade Element and Overall Performance Table Headings	68
5	Blade-Element and Overall Performance Design Data	69
6	Blade-Element and Overall Performance, 50 Percent of Design Speed	70-74
7	Blade-Element and Overall Performance, 70 Percent of Design Speed	75-80
8	Blade-Element and Overall Performance, 90 Percent of Design Speed	81-86
9	Blade-Element and Overall Performance, 100 Percent of Design Speed	87-93

SINGLE-STAGE EVALUATION OF HIGHLY LOADED, HIGH-MACH-NUMBER COMPRESSOR STAGES VI. DATA AND PERFORMANCE CANTILEVERED STATOR

A. S. Merrow Pratt & Whitney Aircraft Division United Aircraft Corporation

SUMMARY

A compressor stage with a rotor tip speed of 1600 ft/sec was tested to evaluate its performance with a cantilevered stator and a rotating inner shroud beneath the stator. Both the rotor blades and the stator vanes were composed of multiple circular arc airfoil sections.

Comparison of data taken during this test of the cantilevered stator and previous tests with the same compressor and airfoil geometry in a shrouded stator configuration showed only slight differences in stage performance with no significant effect on overall efficiency. However, the severity of the stator wake near the rotating hub was decreased at all flows including the near surge condition. Stall and wide open discharge corrected weight flows were the same as for the shrouded stator configuration.

INTRODUCTION

Results from research compressors have shown that compressor rotor blades can be designed to operate with high aerodynamic blade loading and/or high inlet relative Mach number and still achieve good efficiency with acceptable stall margin. There is, however, a severe penalty in stage efficiency due to stator endwall losses.

As part of Contract NAS3-10482, a stator endwall treatment test program was initiated to investigate the effectiveness of various types of endwall treatments for reducing stator losses and increasing the stator stall-free range of operation. The basic compressor stage used for this program had a design rotor tip speed of 1600 ft/sec and demonstrated a stage pressure ratio of 1.946 and a stage efficiency of 84.5 percent. Stator endwall treatments tested previously under this contract included (1) suction through a slit located at the intersection of the stator suction surface and the I.D. wall (Reference 1), (2) blowing from tubes located at the intersection of the stator suction surface and the inner and outer walls (Reference 2), (3) suction through annular slots located in the inner and outer wall at the stator leading edge (Reference 2), and (4) combined blowing and annular suction (Reference 2). To evaluate the effect of these endwall treatments on the stator range, the stator vanes in each test were restaggered four degrees open (increased incidence) with respect to the design stagger. Results indicate however, that the restaggered stator with no endwall treatment is referred to herein as the baseline configuration.

The final configuration to be evaluated is that of a cantilevered stator and rotating inner shroud. The results of tests from this configuration are reported herein.

TEST APPARATUS AND PROCEDURE

TEST COMPRESSOR

The compressor used in this program, Figure 1, was a highly loaded, high Mach number single stage compressor with no inlet guide vanes, 30 MCA rotor blades and 44 MCA stator vanes. It is the same compressor stage used in the work presented in Reference 3 except that a rotating inner shroud and cantilevered stator replaced the shrouded stator. A photograph of the assembled cantilevered stators and rotating inner shroud is shown in Figure 2. The purpose of the rotating shroud was to reduce the boundary layer build up on the inner wall. The original-design stator airfoil sections were restacked on the leading edge to allow the vanes to deflect free of the rotating shroud and the rotating shroud was coated with an abrasive material to insure rapid abrasion of the vanes if rubbing did occur.

The stator vanes were restaggered 4 degrees open, the same as were the vanes of References 1 and 2. The intent of the restagger in previous tests was to promote stator stall from which the effects of endwall treatment could be better evaluated. Results from References 1 and 2 proved that the 4 degree stagger was not sufficient to cause stator stall. The restagger of the stator vanes in the present tests are, however, consistent with Reference 1 and 2. The restaggered shrouded stator with no endwall treatment (Reference 2) is referred to herein as the baseline configuration.

A summary of rotor and stator design geometry is provided in Table 1, including the 4 degree stator restagger. Design details of the basic compressor stage are given in Reference 4. The design aerodynamics are tabulated in Table 5, Appendix 3. Table headings are identified in Table 4, Appendix 3.

INSTRUMENTATION AND CALIBRATION

Axial and circumferential location of instrumentation for measuring aerodynamic performance is shown in Figures 3 and 4. Photographs of typical instrumentation are shown in Figure 5.

Airflow was measured within 1 percent, using a flow nozzle designed to ISA specification. Compressor speed was measured with an electromagnetic pickup that counts the number of gear teeth passing in an interval of time and converts the count into revolutions per minute. Measurement accuracy is better than 0.2 percent of indicated speed between 4,000 rpm and 13,000 rpm.

All temperatures were measured using chromel-alumel Type K thermocouples and recorded in millivolts by the automatic data-acquisition system. Temperature elements were calibrated over their full operating-temperature range for Mach number and total-pressure effects. The thermocouple leads were calibrated for each temperature element. Overall RMS temperature accuracy was estimated to be ±1.0°F.

			`TA	BLE 1	:		
	M	ICA ROTOR	AND STAT	OR DESIGN	PARAMETER	RS	
ROTOR –	STATORS 8 A	ND 9					
% Span	Dia – 1	Dia – 2	β* 8	β* 9	β* 8ss	eta^* sh	Solidit
5 (hub)	17.47	19.77	48.97	1.87	55.40	45.74	2.276
10	18.47	20.41	49.59	9.63	56.02	46.76	2.173
15	19.47	21.05	50.44	16.51	56.59	47.76	2.080
.30	22.31	22.96			57.87	50.53	1.855
50	25.79	25.52	56.40	42.30	59.30	54.68	1.638
70	28.95	28.08	59.08	50.53	61.07	59.17	1.476
85	31.29	29.99	61.63	54.11	62.96	63.01	1.379
90	31.88	30.63	62.53	55.10	63.65	64.18	1.355
95 (tip)	32.50	31.27	63.21	55.84	64.14	64.96	1.332
STATOR -	- STATIONS 1	0 AND 11					
% Span	Dia – 1	Dia – 2	⁻ β* 10	β* 11	β* 10ss	eta^* sh	Solidit
5 (hub)	20.41	21.49	39.23	-16.41	42.15	34.47	2.010
10	21.01	21.96	38.27	-15.44	41.21	32.62	1.959
15	21.59	22.43	37.42	-14.89	40.36	30.94	1.911
30	23.31 .	23.90.	35.44	-15.22	38.44	27.18	1.781
50	25.60	25.89	33.60	-16.04	36.72	24.01	1.632
70	27.82	27.90	32.45	-17.48	35.68	22.38	1.508
85	29.41	29.38	32.12	-19.91	35.44	22.82	1.430
90	29.91	29.86	32.15	-21.40	35.48	23.36	1.407
95 (tip)	30.38	30.29	32.33	-23.69	35.69	24.40	1.387

Disk probes and combination probes were calibrated for Mach number as a function of indicated static-to-total pressure ratio, with pitch angle as a parameter. Total pressure recovery and yaw angle deviation were calibrated as functions of Mach number and pitch angle. Total temperature recoveries for the combination probes were calibrated as functions of Mach number and pitch angle.

All pressures from probes, fixed rakes, and static taps were measured with transducers and recorded in millivolts by the automatic data-acquisition system. The accuracy of the pressure readings was \pm 0.1 percent of the full-scale value.

Instrumentation for overall and blade element performance is listed in Table 2.

TABLE 2 PERFORMANCE AND BLADE ELEMENT INSTRUMENTATION

Instrumentation Location		Parameter	Type and Quantity
Station 0	Plenum chamber	P	6 pressure taps on plenum wall
		T	6 bare-wire thermocouples
-Station 1	Bellmouth instru- mentation ring	p	4 O.D. wall static tap
Station 7	Rotor inlet (within 1/2 chord)	P, p, β	1 disk traverse probe traversed to 9 radial positions*
		p .	4 O.D. and 4 I.D. wall static taps
Station 9.1	Stator inlet instru- mentation plane	P, p, T, β	2 combination probes traversed to 15 radial positions.** (Boundary layer survey only)
Station 10	Stator leading edge	p	4 O.D. and 4 I.D. wall static taps equally spaced and located on extension of midchannel lines
		p	4 O.D. and 4 I.D. wall static taps spaced across one vane gap.
Station 12	Stator exit	P	2 circumferential wake rakes (15 element) traversed to 9 radial positions* (each wake rake spans at least one vane gap at O.D.)
* * * * * * * * * * * * * * * * * * * *	e s	. Т	7 fixed radial rakes each with temperature sensors at 9 radial positions.* 6 rakes spaced circumferentially to obtain readings evenly distributed across a vane gap. The 7th rake is a duplicate of
Cart.	Total		the midgap rake and is 180° from one other midgap rake.
	*	Ρ, p, Τ, β	1 combination probe traversed to 9 radial posi- tions,* 1 combination probe traversed to 15 radial positions** and to 15 tangential positions across one vane gap (Boundary layer survey only)
· · · · · · · · · · · · · · · · · · ·		<u>p</u>	4 O.D. and 4 I.D. wall static taps positioned on an extension of the mid-channel line
•	• ,	: p ***	4 O.D. and 4 I.D. wall static taps spaced across one vane gap

- *The nine radial positions of each axial station are defined by the intersection of the axial station and the design stream lines which pass through 5, 10, 15, 30, 50, 70, 85, 90 and 95 percent of the passage height at the rotor trailing edge.
- **The fifteen radial positions for boundary layer surveys were defined by the intersection of the axial station and design streamlines passing through 2.5, 3.75, 7.5, 92.5, 96.25 and 97.5 percent of the passage height at the rotor trailing edge in addition to the nine radial positions listed above.

Instrumentation which recorded continuously during excursions into stall, including high response hot film probes for detecting rotating stall, is listed in Table 3.

TABLE 3

STALL INSTRUMENTATION

Inlet flow nozzle upstream static pressure Inlet flow nozzle downstream static pressure Inlet flow nozzle ΔP Inlet flow nozzle temperature Plenum total pressure Rotor exit O.D. static pressure Stator exit O.D. static pressure Average rig discharge total pressure Rig mechanical speed

In addition, the following parameters were recorded on one fourteen-channel magnetic tape during the rotating stall survey.

- 4 selected rotor strain gages
- 4 selected stator strain gages
- 3 hotfilm sensors located at the rotor leading edge at 25, 50, and 85 percent of the passage height from the hub.

Stator exit O.D. static pressure

Rig mechanical speed

Proximity and strain gage instrumentation was used to detect excessive stresses and rubbing. Four proximity sensors were mounted on the nonrotating inner duct support to detect axial and radial movements of the rotating shroud. Strain gages were mounted in the rotating inner shroud to measure vibratory hoop and bending stresses. Thermocouples were mounted in the ends of the cantilevered vanes to detect interference between vane and shroud.

TEST PROCEDURE

A brief shakedown test was run to verify the structural integrity of the test apparatus. Levels of vibratory stresses on the blades and vanes and the rotating shroud were recorded during accelerations and decelerations between 50 and 100 percent of design speed with wide open throttle, part throttle, and near stall throttle setting. Two stator vane resonances were encountered, one just above 70 percent of design speed in which peak stresses of 18,000 psi were recorded, and the other near 85 percent of design speed where peak stresses of 24,000 psi were measured. Both speeds were avoided during the remainder of the test program. No interference rubbing between the vanes and rotating parts occurred during the test. Aerodynamic performance tests were then run with uniform inlet flow at speeds of 50, 70, 90, and 100 percent of design speed. Stall flows were measured for each of these speeds. Overall performance was measured at 24 operating points by total pressure wake rakes at nine diameters at the stator trailing edge. The rotor inlet disk probe and one stator exit combination probe was radially traversed to nine positions for 12 of the 24 operating points.

Boundary layer surveys were conducted for 5 of the 24 operating points. A boundary layer survey point is described as one in which two combination probes at the stator inlet were traversed to fifteen radial positions, and one combination probe at the stator exit was traversed tangentially across the stator vane gap at each of the fifteen radial positions. Four boundary layer survey points were taken at 100 percent of design speed, and one point at 90 percent of design speed.

Rotating stall surveys were conducted to determine the point of initiation of rotating stall and the radial extent of the stall zones. As the discharge throttle was closed from wide open to stall for each of the aforementioned speeds, fluctuations in mass flow (ρ Vm) at the rotor inlet were measured by means of a hot film probe having sensors at 25, 50, and 85 percent span from the hub. Measurements from strain gages located on selected rotors and stators, a speed signal, the measurements from a stator exit wall static pressure tap and the mass flow fluctuations measured by the hot film probes were recorded simultaneously on the same recording device.

CALCULATION PROCEDURES

Data were aerodynamically corrected and mass flow averaged in the same manner as discussed in Reference 3 (uniform inlet flow). Overall performance and blade element calculations (Appendix 1) were made using stator exit total pressure wake rake data.—Blade-element data—were calculated by a flowfield calculation program and used peak wake rake values from stator exit wake rakes to describe the rotor exit pressure. For comparative purposes, data from the stator exit combination probes which were traversed both tangentially and radially during the boundary layer surveys, were also used to calculate overall performance.

Contour plots of total and static pressure, air angle, meridional velocity, and total temperature were generated from stator exit tangential and radially traversed probe measurements. Meridional velocity was calculated from the absolute velocity using the measured yaw angle and assumed design pitch angle. The absolute velocity was calculated from the measurement of total and static pressure and total temperature.

RESULTS AND DISCUSSION

The results of the centilevered stator test are presented in the form of overall performance, stator gapwise distributions of total pressure, blade element performance and contour plots of stator survey data.

In an effort to evaluate the effects of the cantilevered stator (rotating hub) on stage performance, it is necessary to make some comparisons of data from the cantilevered stator configuration to that from the baseline configuration (restaggered shrouded stator with no endwall treatment) reported in Reference 2. The comparisons are based on overall performance, stage spanwise distributions of total pressure ratio and efficiency near the peak efficiency point at design speed, and blade element total loss parameter for 5, 10, 15, 30 and 50 percent span locations at design speed.

All data from the cantilevered stator configuration are presented in tabular form in Appendix 3. All of the baseline data are presented in tabular form in Reference 2.

Overall Performance

Overall rotor and stage performance are presented in Figures 6 and 7 respectively for the cantilevered and baseline (Reference 2) stator configurations. The solid lines and circles represent the baseline data and the square symbols represent the data from the cantilevered stator configuration. There is a slight difference in rotor overall performance for the cantilevered stator configuration as compared to the baseline data (Figure 6). However, the rotor exit total pressure is based on the peak wake rake pressure at the stator exit and could be affected by changes in the gapwise distribution of total pressure in the vicinity of the rotating hub. Stage overall performance comparisons between the cantilevered and baseline configurations are shown in Figure 7.

The comparison shows practically no difference in overall stage performance for 50, 70, and 100 percent design speed, but shows a slight improvement in efficiency (1 to 1-½ points) for the 90 percent speed. The stall limit line is identical for the two configurations.

A comparison of spanwise distribution of stage overall performance for the baseline and cantilevered stator configurations is presented in Figure 8 at the near peak efficiency condition for design speed. This data is from the boundary layer survey instrumentation (tangential and radially traversed combination probes at the stator exit) and shows no significant changes in the spanwise distribution of stage performance for the two configurations at peak efficiency conditions.

Stator Exit Gapwise Distribution of Total Pressure

Stator exit gapwise total pressure comparisons are presented in Figures 9, 10 and 11 for near surge, peak efficiency and wide open throttle conditions. Severity of stator vane wakes near the hub is decreased with the cantilevered stator. At five percent span, peak to peak variation of the wake is decreased approximately 40 percent at all flow conditions. The effect is limited to the 10 percent of span nearest the hub. From 10 percent span outward, the total pressure profile is changed slightly, but the severity of the stator wake remains the same for both cantilevered and shrouded configurations. The rotating hub could be beneficial for following blade rows in a multistage application, and could improve stage stall range in cases where stall range is limited by stator hub stall.

Blade Element Performance

Blade element total pressure loss coefficient, diffusion factor and deviation angle versus suction surface incidence are presented at 50, 70, 90 and 100 percent design speed for the rotor and stator in Figures 12 and 13 respectively. The data are also included in tabular form in Appendix 3. At 100 percent design speed, plots of total loss parameter versus suction surface incidence angle are compared for the baseline and cantilevered stator configurations. The comparisons are made for the 5, 10, 15, 30 and 50 percent span elements and are presented in Figures 14 and 15 for rotor and stator respectively.

The rotor blade element loss parameter for the cantilevered stator configurations differs substantially from that of the baseline configuration at the 5, 10, and 15 percent span locations (Figure 13). There are no substantial differences in the rotor loss parameter incidence angle characteristics for the configurations at 30 and 50 percent span locations. The change in incidence angle loss characteristics of the rotor for the 5, 10 and 15 percent span locations is a result of the change in the circumferential distribution of total pressure behind the stator vanes due to the rotating hub (cantilevered stator configuration).

The blade element total loss parameter for the cantilevered stator is substantially different from that of the baseline stator configuration (Figure 15) for the 5, 10, and 15 percent span locations. There are no substantial differences in stator loss parameter incidence angle characteristics for the 30 and 50 percent span locations. The change in the loss parameter incidence angle characteristic for the two stator configurations is again the result of the change in circumferential distribution of stator exit total pressure due to the rotating stator hub.

A change in the circumferential distribution of the stator exit total pressure affects both the rotor and stator blade element data because (as discussed in the Calculation Procedure) the peak wake rake pressure at the stator exit is used for the rotor exit and stator inlet total pressure. Therefore, both rotor and stator diffusion factors, losses and rotor deviation angle, and stator incidence angle are affected by a change in the circumferential distribution of stator exit total pressure.

Contour Plots at Stator Exit

Tangential traverses were made at the stator exit for part throttle, maximum efficiency and near stall operating points at design speed and at the near stall point at 90 percent of design speed. Measurements of total and static pressure, total temperature, and absolute air angle were recorded at 3.8, 4.9, 5, 9, 8.4, 11.0, 15.4, 31.0, 51.2, 72.7, 87.8, 92.8, 94.1, 95.3, 96.6, and 97.4 percent of passage height from the hub. Tangential spacing gave 15 readings across a stator gap at about 90 percent span and 11 readings at about 4 percent span. These measurements were used to calculate velocity vectors and to construct contour plots showing patterns of pressure and temperature ratio, airflow angle, and meridional velocity at the stator exit instrumentation plane. These contours are shown in Figures 16 through 20.

Rapid Response Hot-Film Data

Traces of hot film probe measurements of rotor leading edge pressure fluctuations during a 100 percent design speed surge are shown in Figure 21. The tip region appears to stall slightly sooner than the midspan or hub region. Duration of the surge pulse was 0.13 sec. No obvious rotating stall pattern was seen.

SUMMARY REMARKS

The overall stage performance for the cantilevered stator configuration showed no significant improvements over that for the baseline configuration. Increased gapwise mixing near the rotating hub reduced the circumferential variation of flow conditions near the hub, but the radial profiles of circumferentially mass averaged pressure ratio and efficiency were nearly identical to those obtained with the baseline stator. However, the severity of the stator wake near the rotating hub was decreased at all flows including the near surge condition. This could be of some benefit in following blade rows in a multistage application or could possibly improve stage range in those cases where stage range is controlled by stator hub stall.

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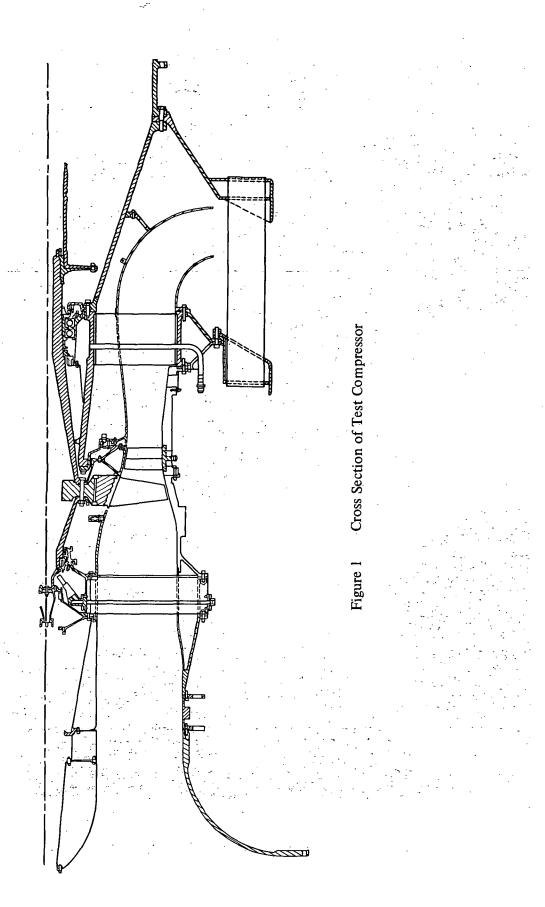




Figure 2 Cantilevered Stator and Rotating Shroud Assembly

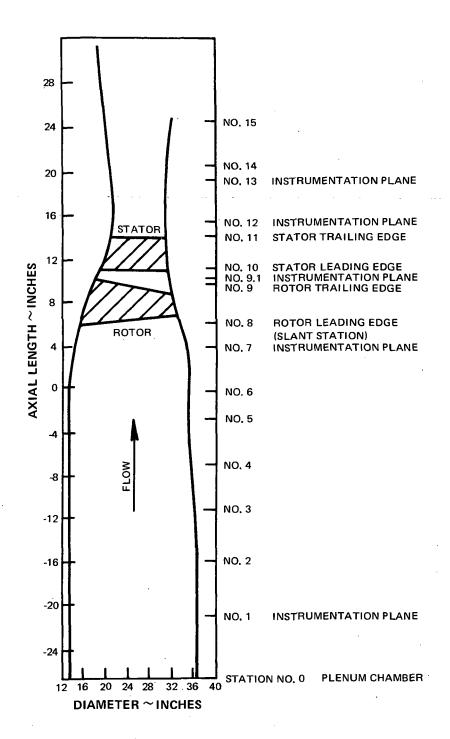


Figure 3 Axial Station Number Designation and Location of Instrumentation

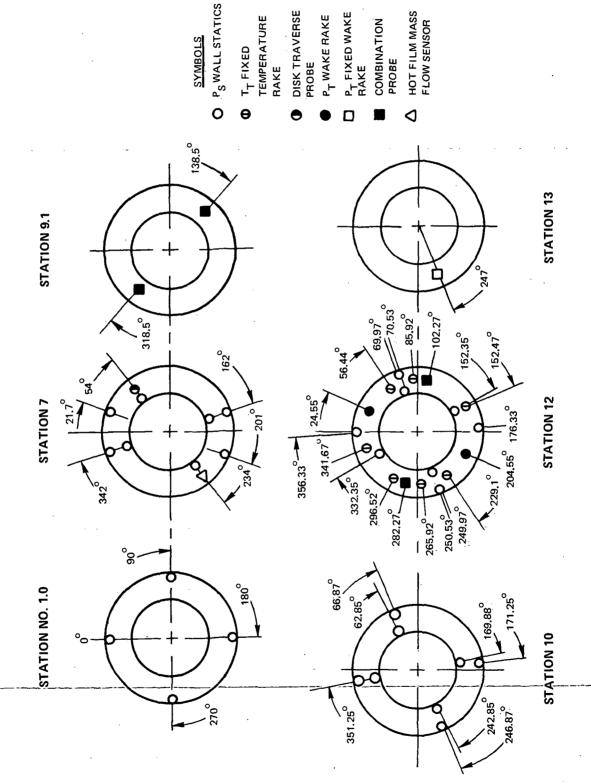


Figure 4 Circumferential Location of Instrumentation, Viewed From Rear

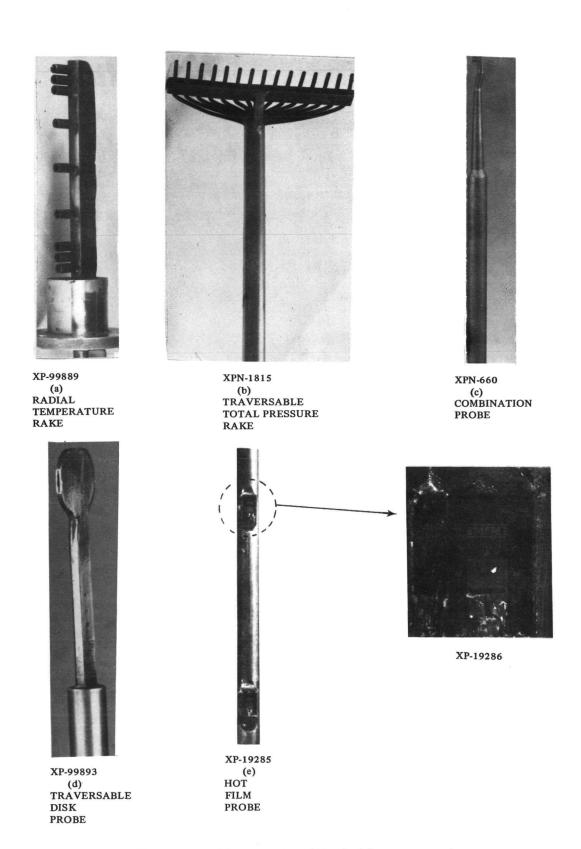


Figure 5 Photographs of Typical Instrumentation

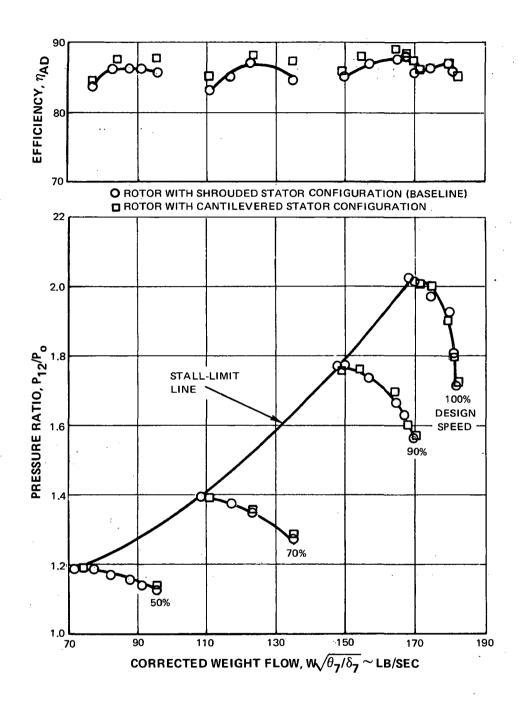
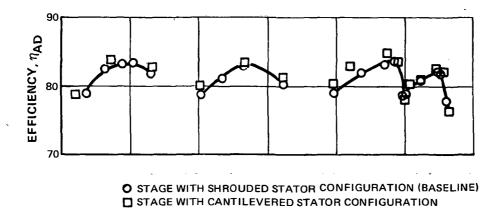


Figure 6 Rotor Overall Performance Comparison
Cantilevered Versus Shrouded Stator



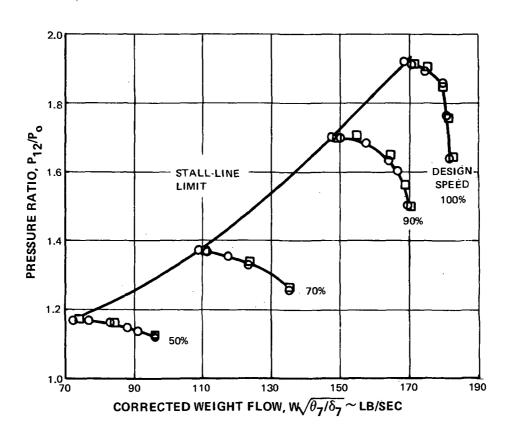


Figure 7 Stage Overall Performance Comparison Cantilevered Versus Shrouded Stator

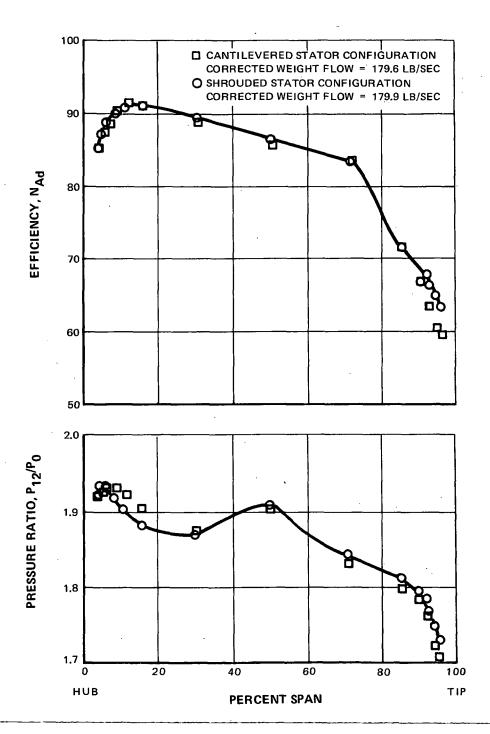


Figure 8 Comparison of Stage Spanwise Performance
Cantilevered Versus Shrouded Stator
Tangential Probe Data - 100 Percent Design Speed

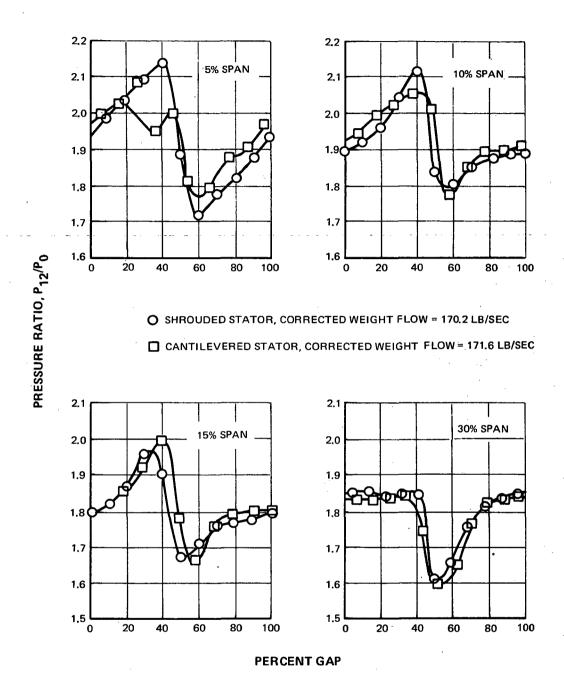


Figure 9 Stator Exit Gapwise Total Pressure Distribution, Cantilevered Versus Shrouded Stator Near Stall Flow Condition, 100 Percent Design Speed

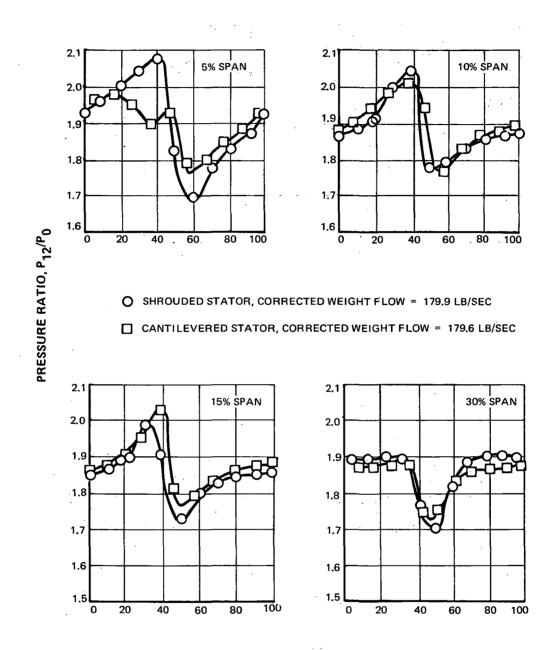


Figure 10 Stator Exit Gapwise Total Pressure Distribution, Cantilevered Versus Shrouded Stator Peak Efficiency Flow Conditions, 100 Percent Design Speed

PERCENT GAP

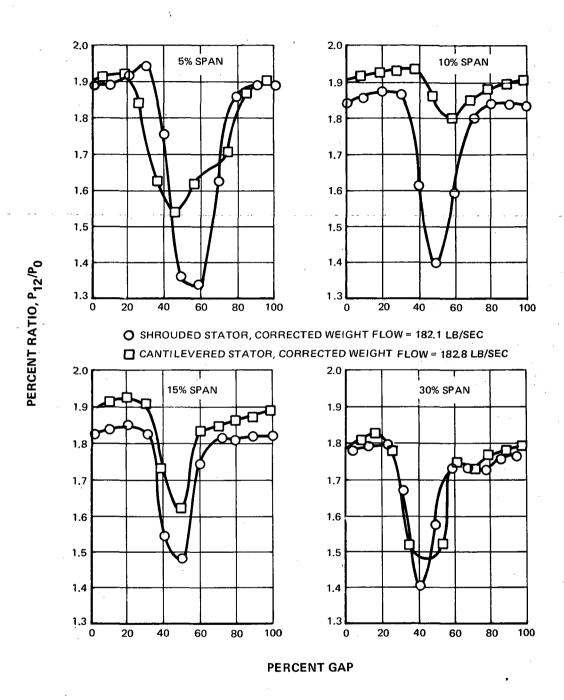


Figure 11 Stator Exit Gapwise Total Pressure Distribution, Cantilevered Versus Shrouded Stator Wide Open Throttle Condition, 100 Percent Design Speed

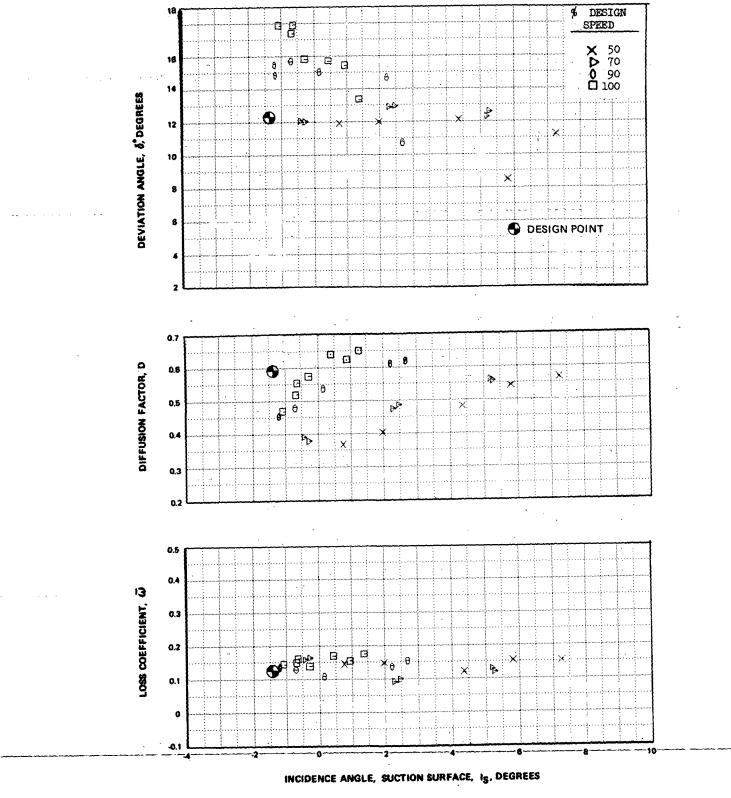


Figure 12a Rotor Blade Element Performance, 5% Span

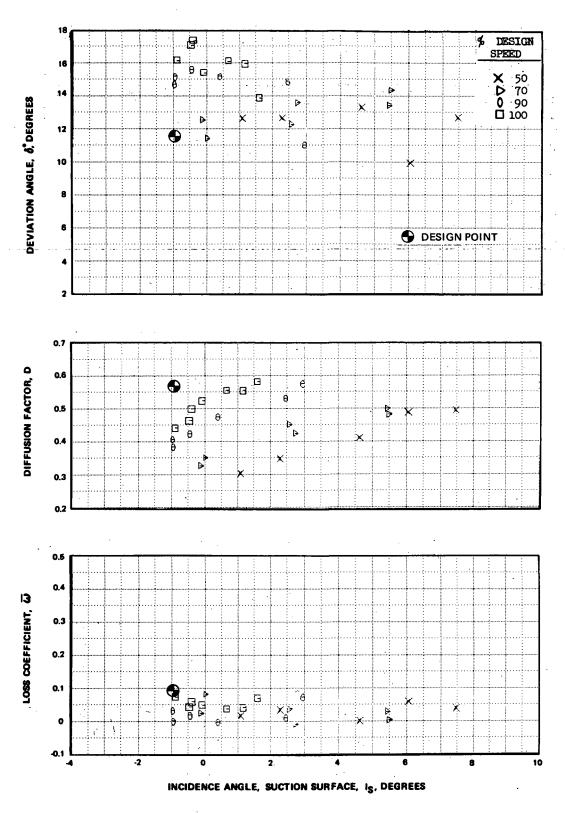


Figure 12b Rotor Blade Element Performance, 10% Span

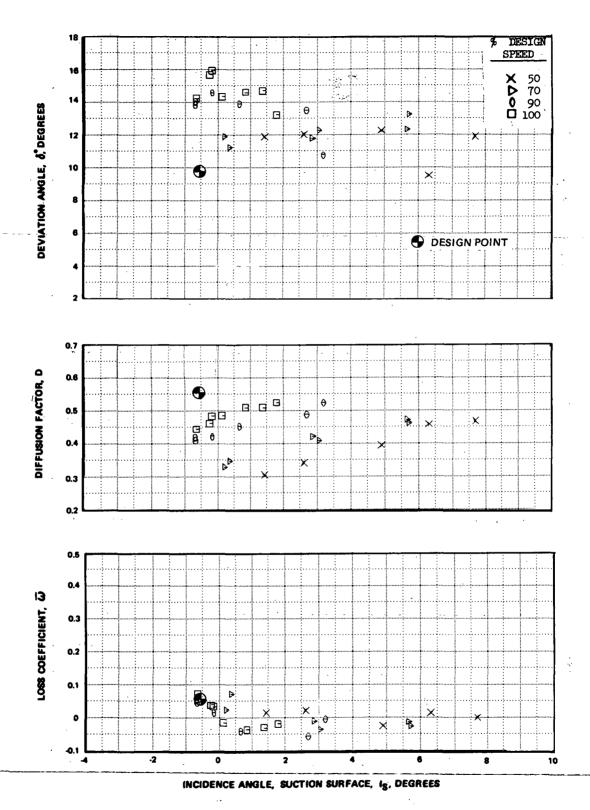


Figure 12c Rotor Blade Element Performance, 15% Span

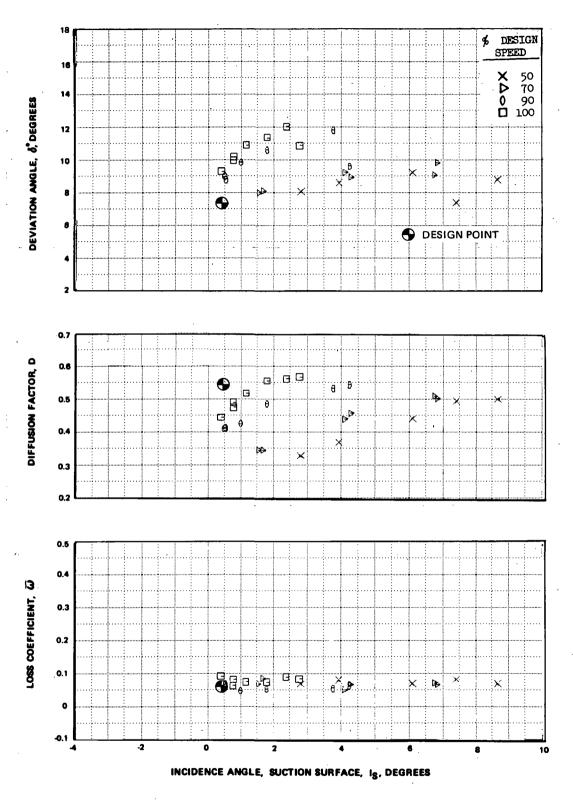


Figure 12d Rotor Blade Element Performance, 30% Span

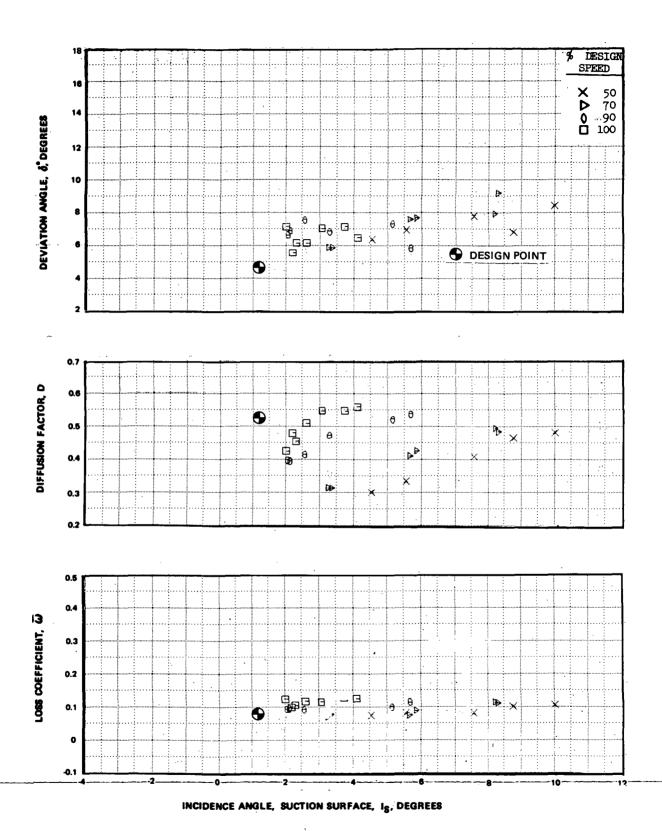


Figure 12e Rotor Blade Element Performance, 50% Span

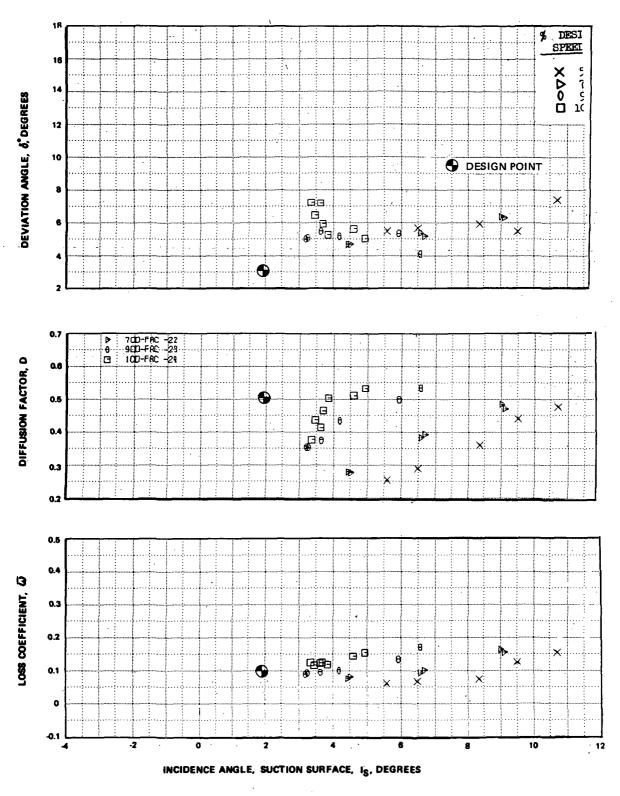


Figure 12f Rotor Blade Element Performance, 70% Span

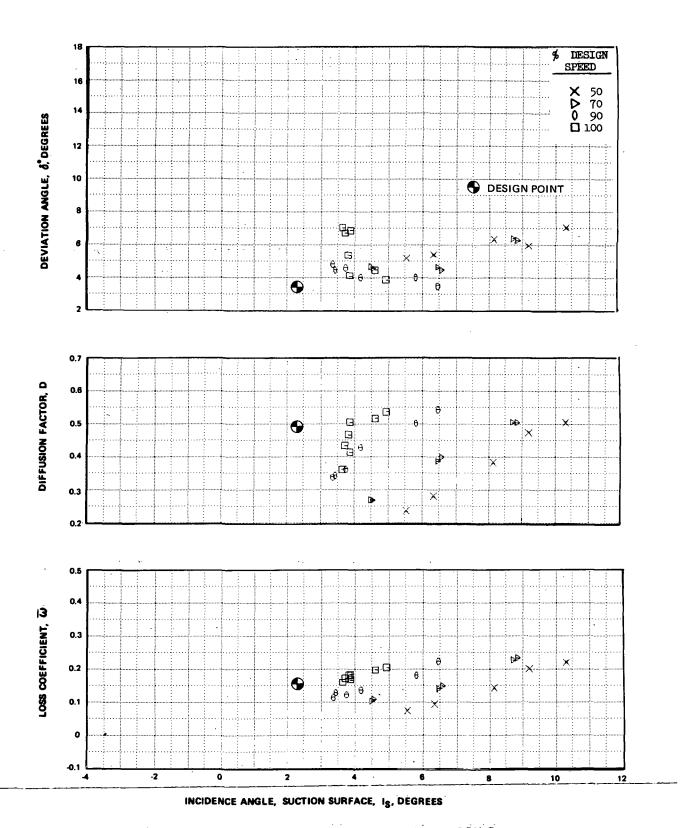


Figure 12g Rotor Blade Element Performance, 85% Span

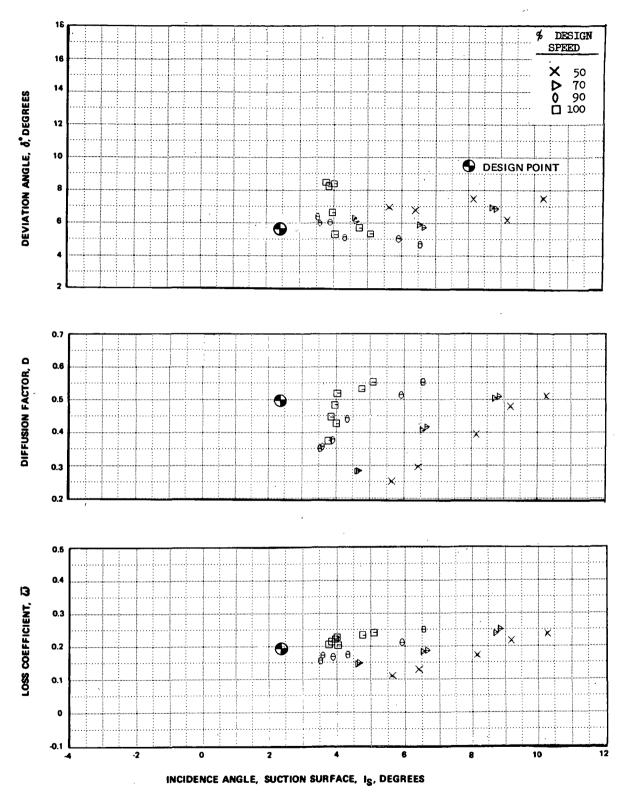


Figure 12h Rotor Blade Element Performance, 90% Span

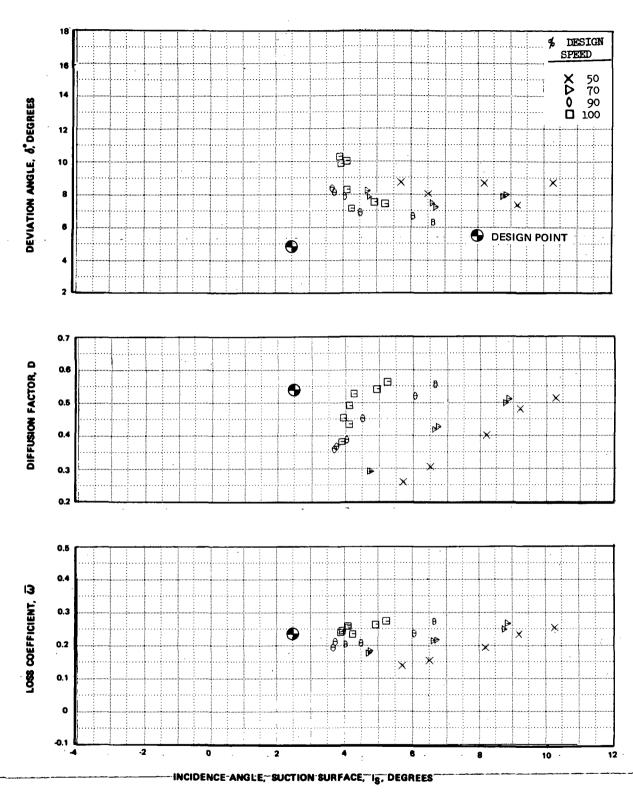


Figure 12i Rotor Blade Element Performance, 95% Span

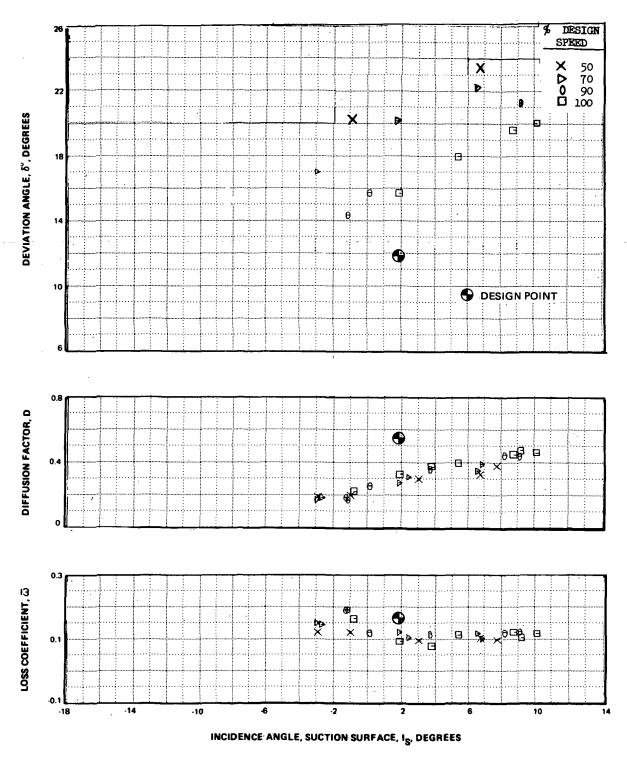


Figure 13a Stator Blade Element Performance, 5% Span

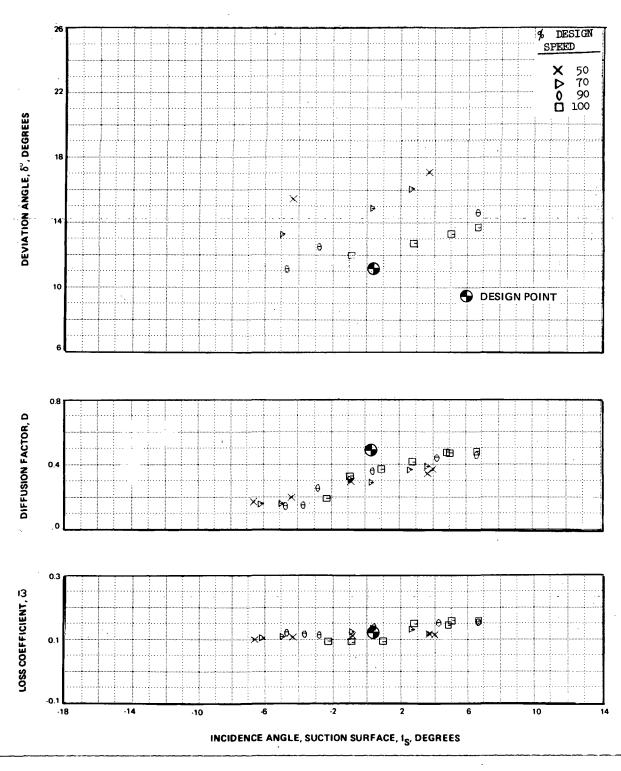


Figure 13b Stator Blade Element Performance, 10% Span

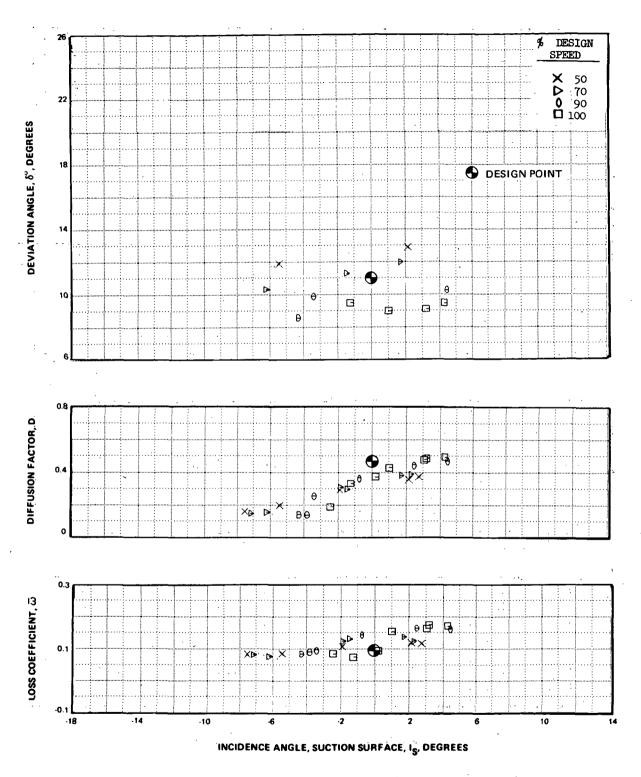


Figure 13c Stator Blade Element Performance, 15% Span

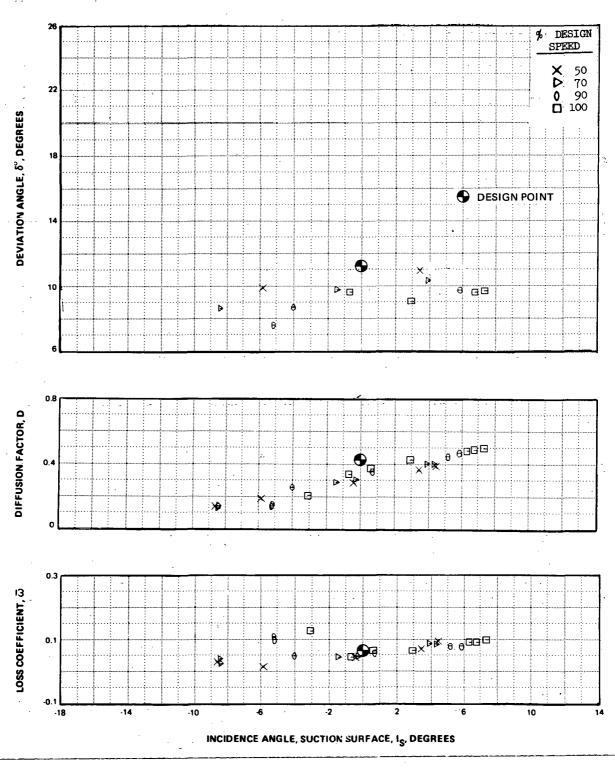


Figure 13d Stator Blade Element Performance, 30% Span

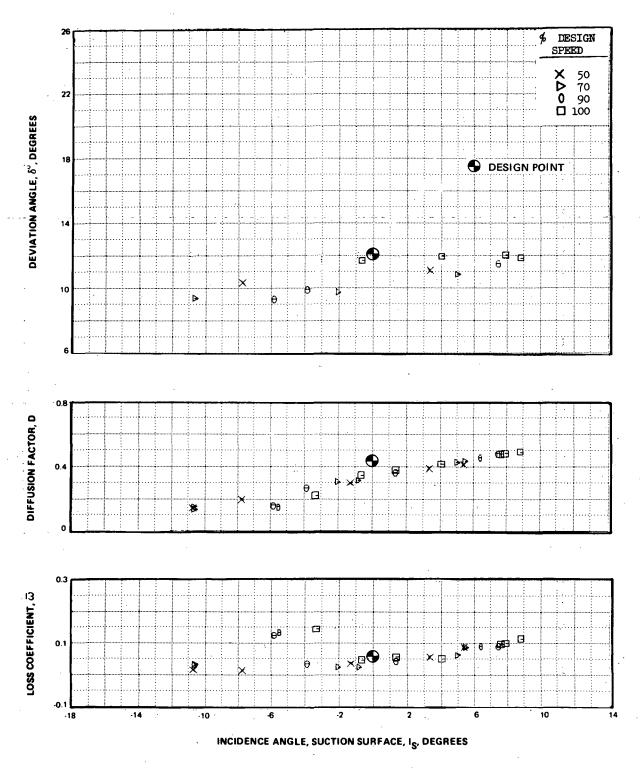


Figure 13e Stator Blade Element Performance, 50% Span

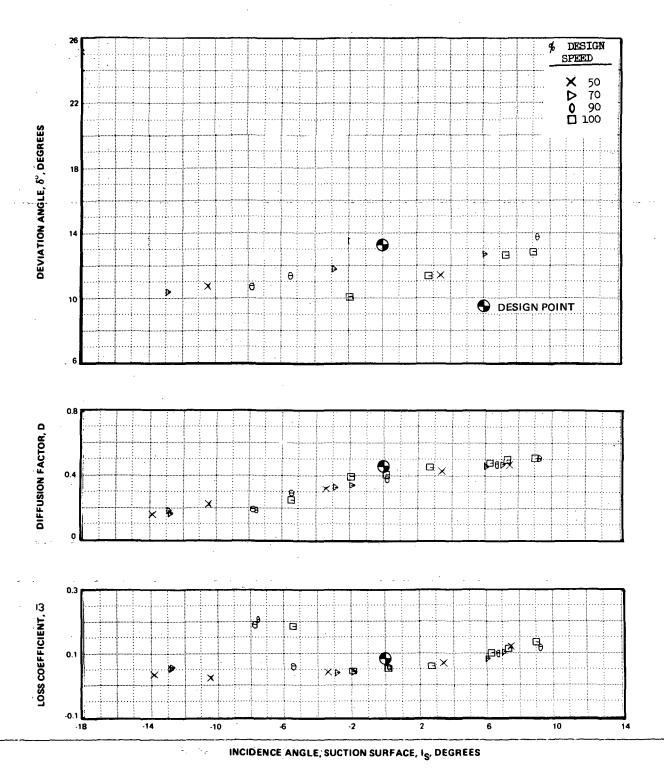


Figure 13f Stator Blade Element Performance, 70% Span

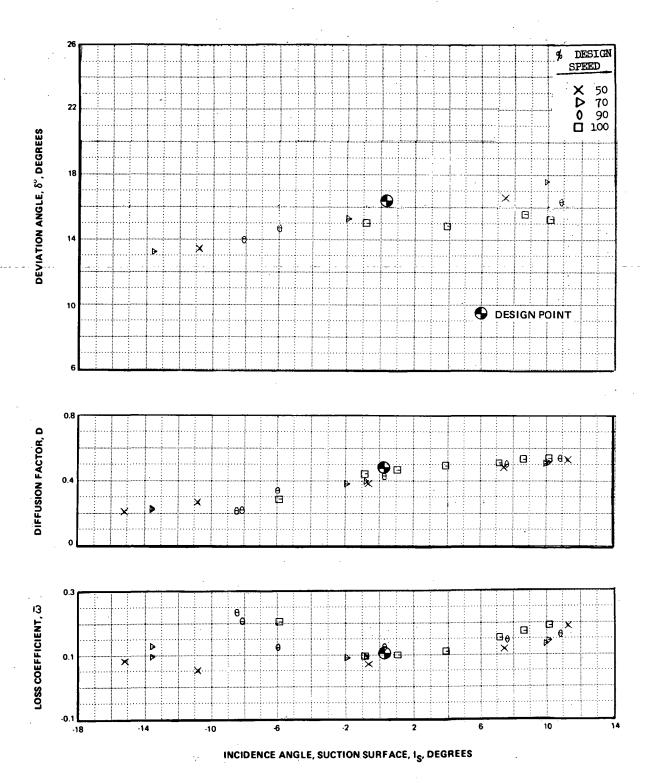


Figure 13g Stator Blade Element Performance, 85% Span

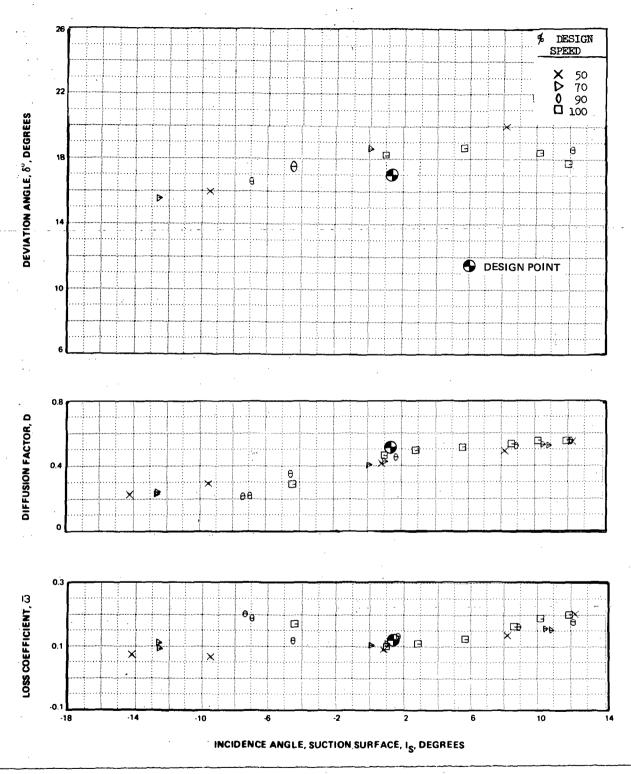


Figure 13h Stator Blade Element Performance, 90% Span

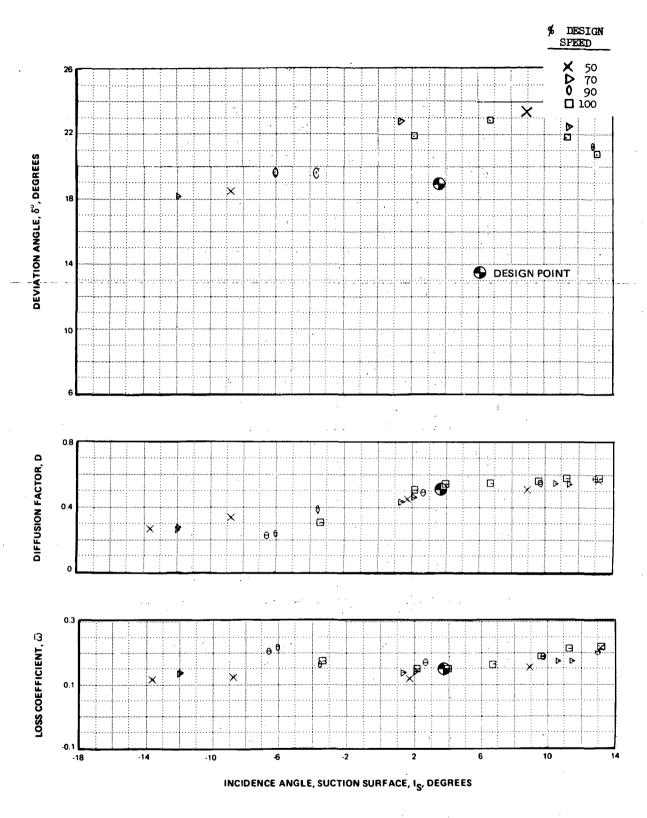


Figure 13i Stator Blade Element Performance, 95% Span

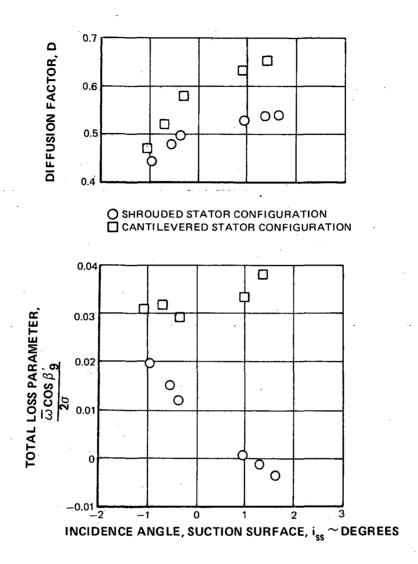


Figure 14a Rotor Blade Element Performance, Cantilevered Versus Shrouded Stator - 5 Percent Span at Design Speed

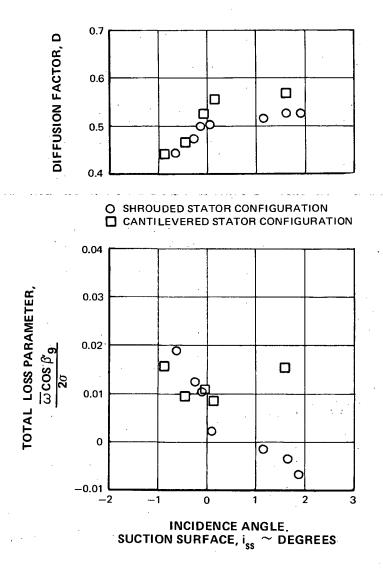
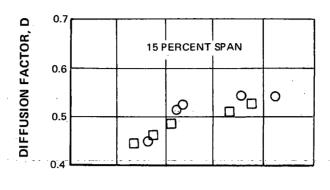


Figure 14b Rotor Blade Element Performance, Cantilevered Versus Shrouded Stator – 10 Percent Span at Design Speed



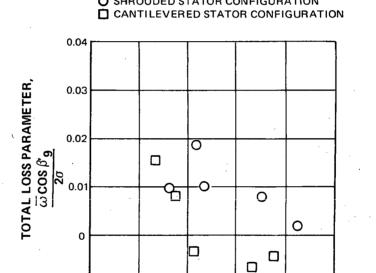


Figure 14c Rotor Blade Element Performance, Cantilevered Versus Shrouded Stator -15 Percent Span at Design Speed

INCIDENCE ANGLE, SUCTION SURFACE, i_{ss} ~ DEGREES

-0.01<u>-</u>2

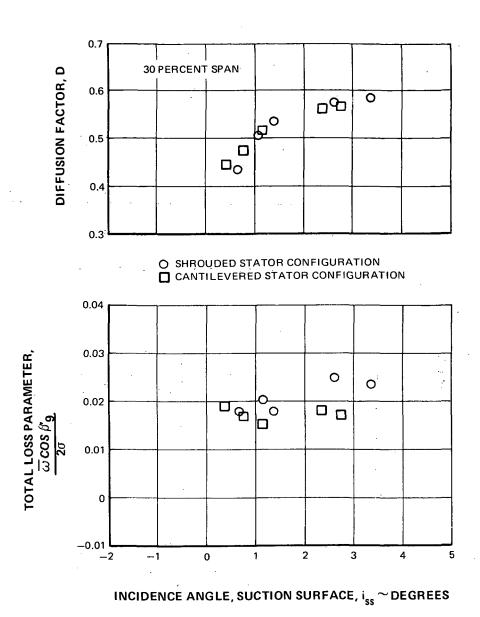


Figure 14d Rotor Blade Element Performance, Cantilevered Versus Shrouded Stator – 30 Percent Span at Design Speed

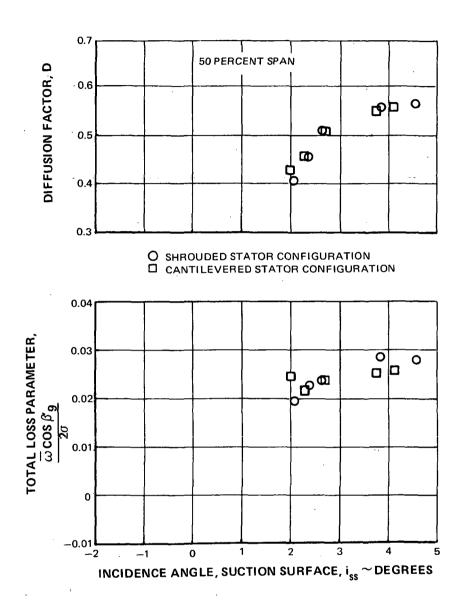
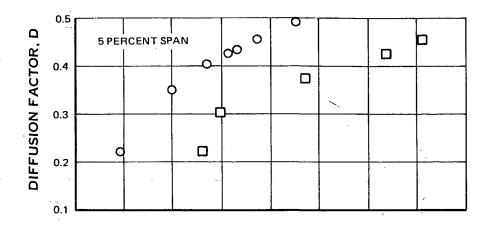
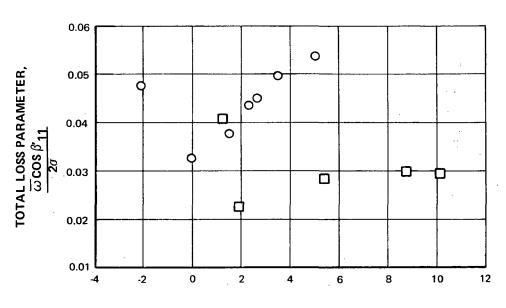


Figure 14e Rotor Blade Element Performance, Cantilevered Versus Shrouded Stator - 50 Percent Span at Design Speed



O SHROUDED STATOR CONFIGURATION

CANTILEVERED STATOR CONFIGURATION



- INCIDENCE ANGLE, SUCTION SURFACE, $i_{\rm SS} \simeq {\rm DEGREES}$

Figure 15a Stator Blade Element Performance, Cantilevered Versus Shrouded Stator — 5 Percent Span at Design Speed

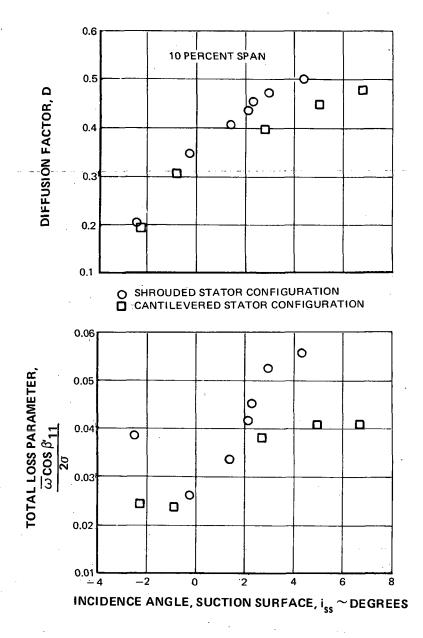


Figure 15b Stator Blade Element Performance, Cantilevered Versus Shrouded Stator -10 Percent Span at Design Speed

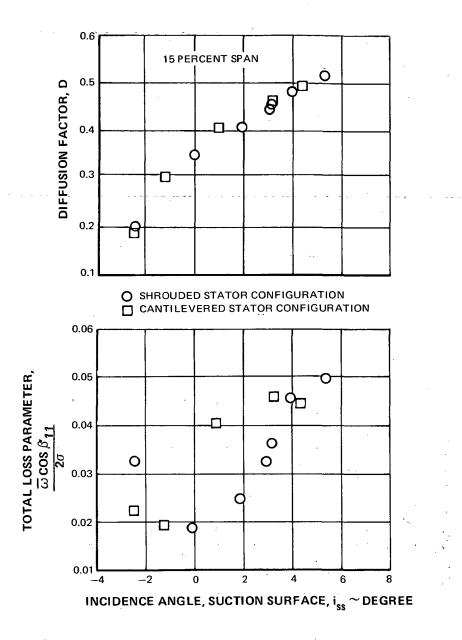


Figure 15c Stator Blade Element Performance, Cantilevered Versus Shrouded Stator -15 Percent Span at Design Speed

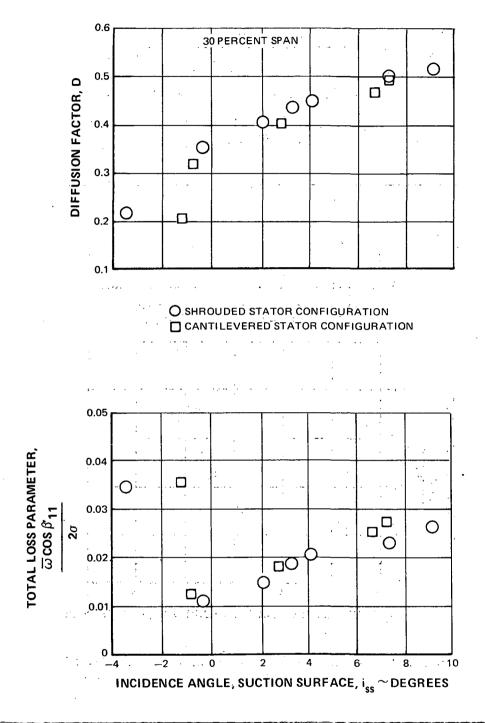


Figure 15d Stator Blade Element Performance, Cantilevered Versus Shrouded Stator – 30 Percent Span at Design Speed

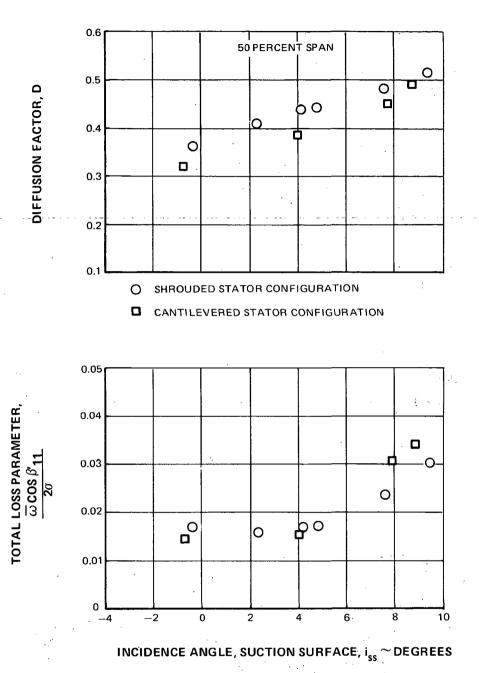


Figure 15e Stator Blade Element Performance, Cantilevered Versus Shrouded Stator – 50 Percent Span at Design Speed

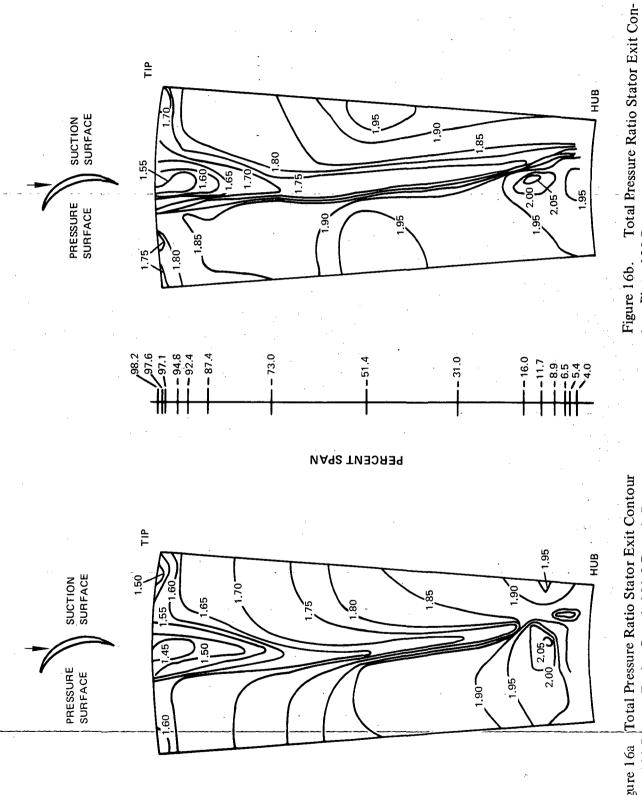


Figure 16a Total Pressure Ratio Stator Exit Contour Plots, 100 Percent Design Speed, 181.3 Pounds Per Second Flow Rate

tour Plots, 100 Percent Design Speed, 179.6 Pounds

Per Second Flow Rate

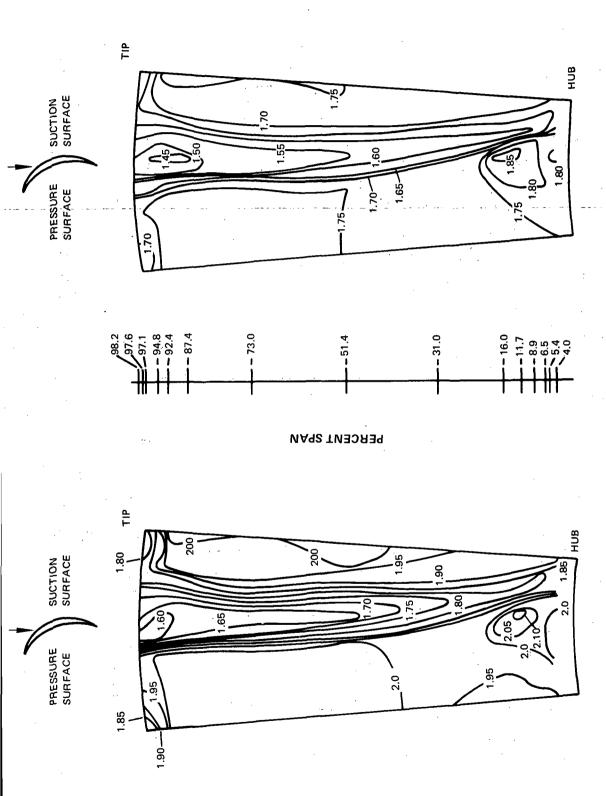
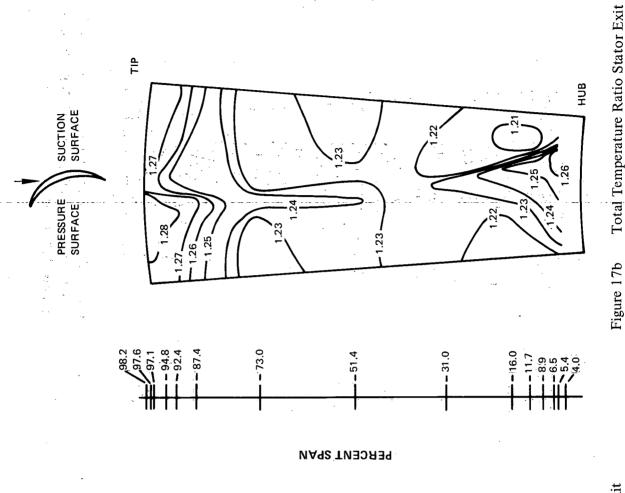


Figure 16c. Total Pressure Ratio Stator Exit Contour Plots, 100 Percent Design Speed, 171.6 Pounds Per Second Flow Rate

Figure 16d Total Pressure Ratio Stator Exit Contour Plots, 90 Percent Design Speed, 149.2 Pounds
Per Second Flow Rate



08

05

1.22

1.25

Figure 17a Total Temperature Ratio Stator Exit Contour Plots, 100 Percent Speed, 181.3 Pounds Per Second Flow Rate

Contour Plots, 100 Percent Speed, 179.6 Pounds Per

Second Flow Rate

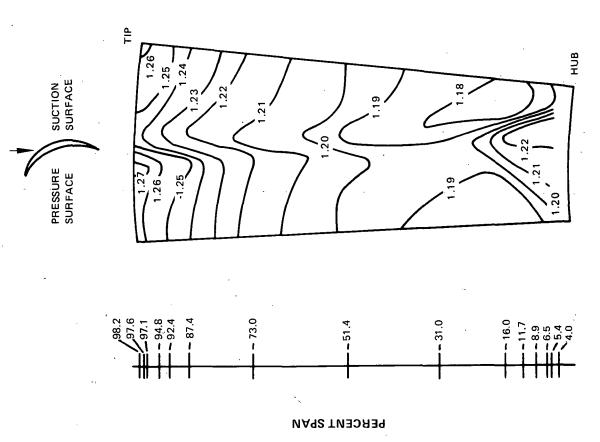
HUB

2,4

SUCTION SURFACE

PRESSURE SURFACE

르



H

1.29

1.28

1.31

SUCTION SURFACE

PRESSURE SURFACE



HUB

1.22

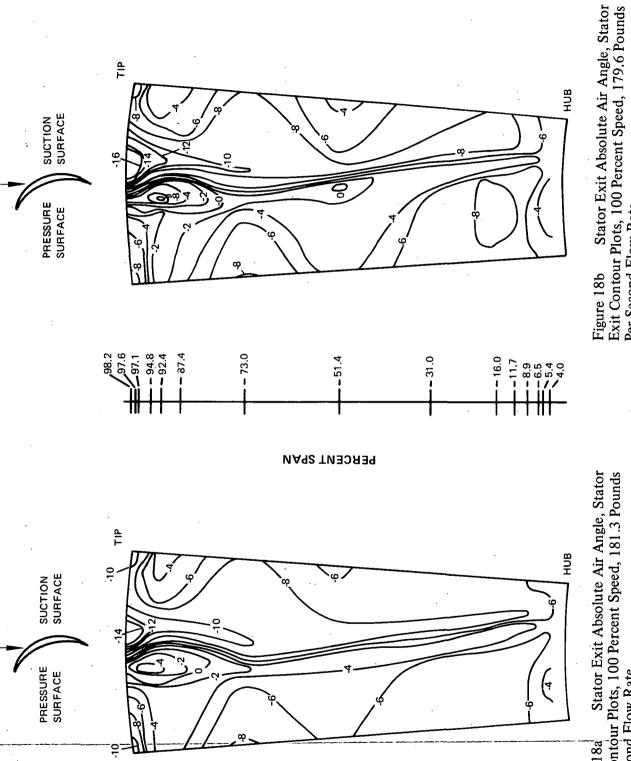
1.23

Total Temperature Ratio Stator Exit

Figure 17d

Contour Plots, 90 Percent Speed, 149.2 Pounds Per Second Flow Rate





Exit Contour Plots, 100 Percent Speed, 181.3 Pounds Per Second Flow Rate Stator Exit Absolute Air Angle, Stator Figure 18a

Per Second Flow Rate

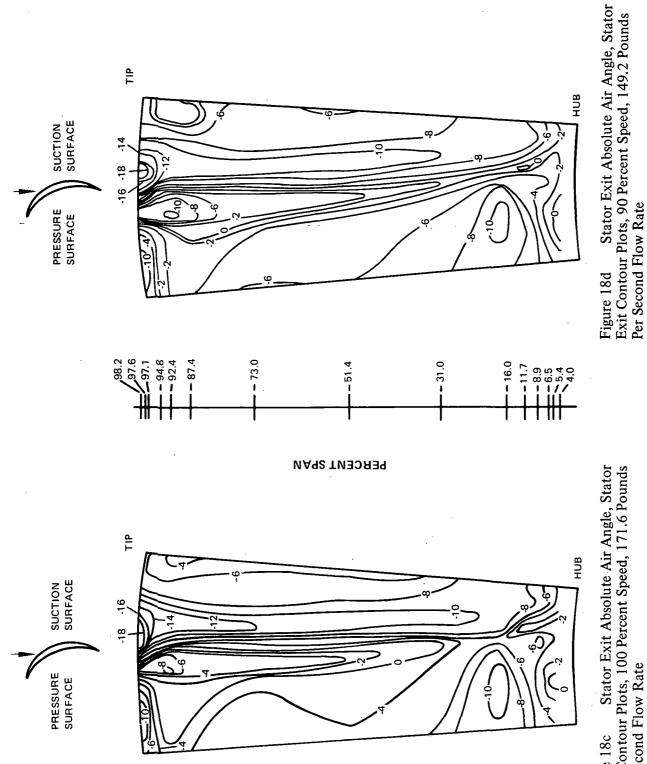
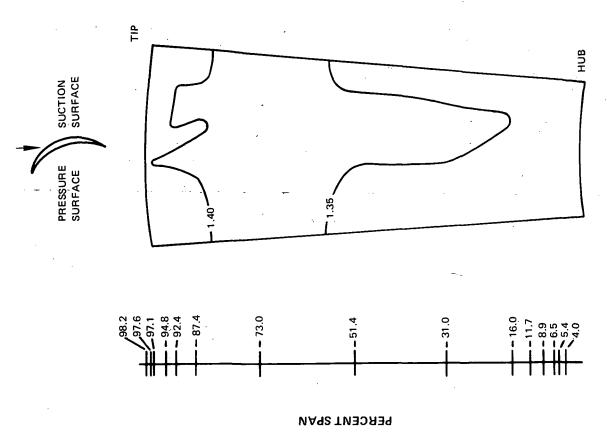


Figure 18c Stator Exit Absolute Air Angle, Stator Exit Contour Plots, 100 Percent Speed, 171.6 Pounds Per Second Flow Rate

Figure 19a Static Pressure Ratio, Stator Exit Contour Plots, 100 Percent Speed, 181.3 Pounds Per Second Flow Rate



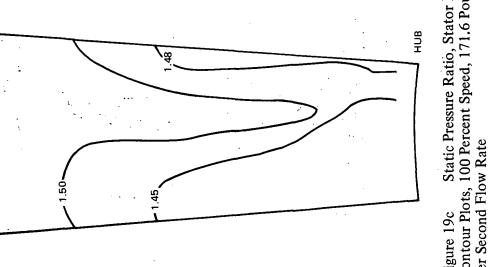
ᆸ

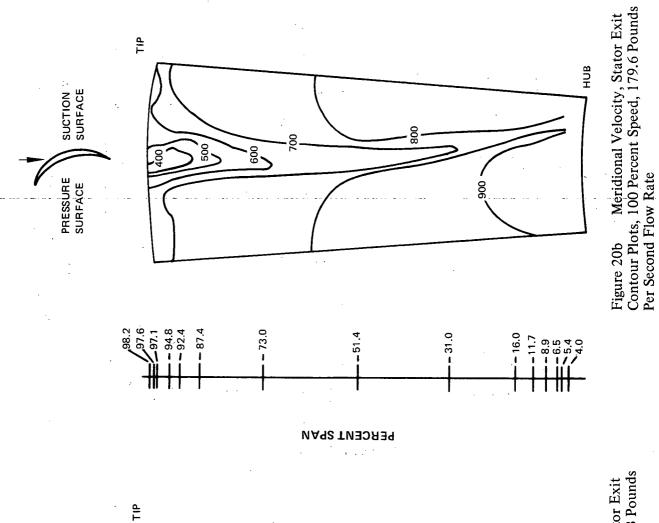
SUCTION SURFACE

PRESSURE SURFACE



Figure 19d Static Pressure Ratio, Static Exit Contour Plots, 90 Percent Speed, 149.2 Pounds Per Second Flow Rate





800

Figure 20a Meridional Velocity, Stator Exit Contour Plots, 100 Percent Speed, 181.3 Pounds Per Second Flow Rate

HUB

1,000,1

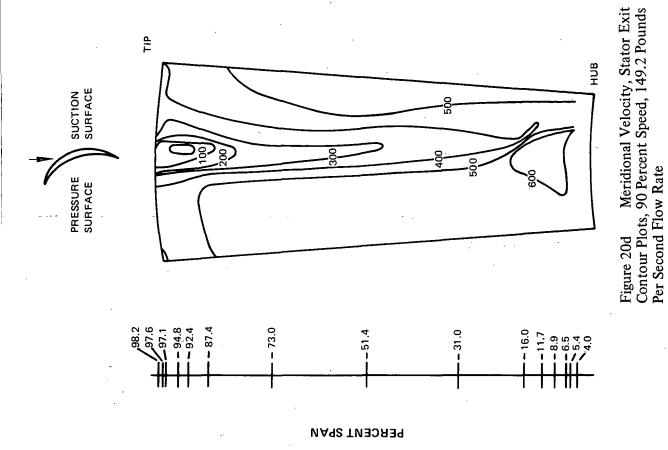
_ اق

1,000

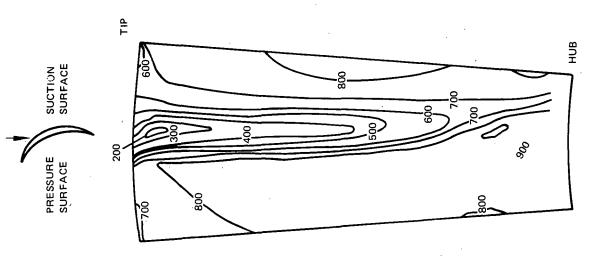
SUCTION SURFACE

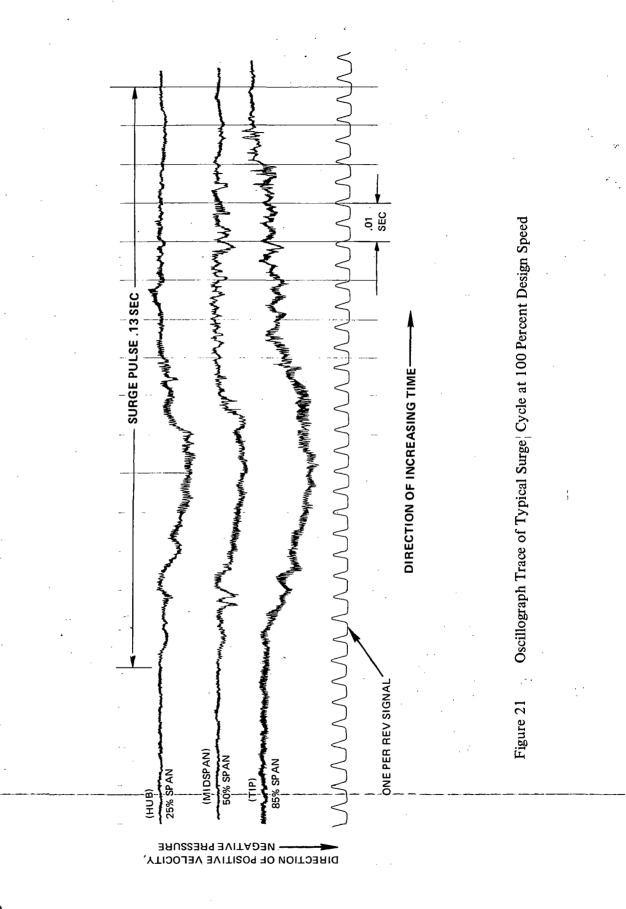
PRESSURE SURFACE 100

400









APPENDIX 1

PERFORMANCE PARAMETERS

a) Relative total temperature

$$T'_{8} = t_{8} \left[1 + \frac{\gamma - 1}{2} (M'_{8})^{2} \right]$$
 (rotor in)
 $T'_{9} = T'_{8} + \left[\frac{(\omega r_{8})^{2} - (\omega r_{9})^{2}}{\frac{2\gamma}{\gamma - 1} Rg_{c}} \right]$ (rotor out)

b) Incidence angle based on mean camber line

$$i_{m} = \beta'_{8} - \beta'^{*}_{8}$$
 (rotor)
 $i_{m} = \beta_{10} - \beta^{*}_{10}$ (stator)

c) Deviation

$$\delta^{\circ} = \beta_{19}^{\circ} - \beta_{18}^{\circ}$$
 (rotor)
$$\delta^{\circ} = \beta_{11}^{\circ} - \beta_{11}^{\ast}$$
 (stator)

d) Diffusion factor

$$D = 1 - \frac{V'_{9}}{V'_{8}} + \frac{r_{9}V_{\theta 9} - r_{8}V_{\theta 8}}{(r_{8}+r_{9}) \sigma V'_{8}}$$

$$D = 1 - \frac{V_{11}}{V_{10}} + \frac{r_{10}V_{\theta 10} - r_{11}V_{\theta 11}}{(r_{10} + r_{11}) \sigma V_{10}}$$
(stator)

e) Loss coefficient

$$\overline{\omega} = \frac{P'_8 \left[\frac{T'_9}{T'_8}\right] \frac{\gamma}{\gamma - 1}}{P'_8 - P'_8}$$

$$\overline{\omega} = \frac{P_{10} - P_{11}}{P_{10} - P_{10}}$$
(rotor)
$$(stator)$$

f) Loss parameter

$$\frac{\overline{\omega}\cos\beta'9}{2\sigma}$$
 (rotor)

$$\frac{\overline{\omega}\cos\frac{\beta}{11}}{2\sigma}$$
 (stator)

g) Polytropic efficiency

1)
$$\eta_{p} = \frac{-\frac{\gamma - 1}{\gamma} \ln \left[\frac{P_{9}}{P_{7}} \right]}{\ln \left[\frac{T_{9}}{T_{0}} \right]}$$
 (rotor)

2)
$$\eta_{p} = \frac{\frac{\gamma - 1}{\gamma} \ln \left[\frac{p_{11}}{p_{10}}\right]}{\ln \left[\frac{t_{11}}{t_{10}}\right]}$$
 (stator)

h) Adiabatic efficiency

$$\eta_{\text{ad}} = \frac{\begin{bmatrix} P_9 \\ P_7 \end{bmatrix} \frac{\gamma - 1}{\gamma}}{\begin{bmatrix} T_{12} \\ T_0 \end{bmatrix} - 1}$$
(rotor)

$$\eta_{\text{ad}} = \frac{\begin{bmatrix} \frac{P_{12}}{P_7} \end{bmatrix} \frac{\gamma - 1}{\gamma}}{\begin{bmatrix} \frac{T_{12}}{T_0} \end{bmatrix} - 1}$$
(stage)

i) Wake blockage factor

$$\vec{K} = \frac{\sum_{i=\rho}^{n} AV}{n} / \rho AV_{avg}$$

where n is number of tangential traverse points equally spaced across a stator gap and ρAV avg is calculated from mass flow averaged values of P, p, and T at that radius

APPENDIX 2

SYMBOLS

area, ft² annulus area, ft² frontal area, ft² A_f С chord length, in D diffusion factor conversion factor, 32.17 lb_mft/lb sec² g_{c} incidence angle, angle between inlet air direction and line tangent to blade im mean camber line at leading edge, degrees (labelled INCM, Table 4) - incidence angle, angle between inlet air direction and line tangent to blade is suction surface at leading edge, degrees (labelled INCS, Table 4) - Mach number M - rotor speed, rpm (N/ $\sqrt{\theta}$ labelled NCOR, Table 4) N P total pressure, psfa static pressure, psfa p radius, ft - gas constant for air, ft lb/lb_m R S blade spacing, in Т total temperature, °R static temperature, °R t t/c thickness-to-chord ratio

V - air velocity, ft/sec

rotor speed, ft/sec

Vm - meridional velocity (Vr² + Vz²) 1/2, ft/sec (labelled VM, Table 4)

W - weight flow, lbs/sec

 β - absolute air angle, $\cot^{-1} (Vm/V \theta)$, degrees (labelled B, Table 4)

 β' - relative air angle, $\cot^{-1} (Vm/V \theta)$, degrees (labelled B', Table 4)

 γ - ratio of specific heats for air, 1.4

Δβ - air turning angle, degrees

 $\Delta \beta^*$ - camber angle, degrees

δ - ratio of inlet total pressure to standard pressure of 2116.22 lbs/ft²

 δ° - deviation angle, angle between exit air direction and tangent to blade mean camber line at trailing edge, degrees

 ϵ - angle between tangent to streamline projected on meridional plane and axial direction, degrees

 η - efficiency, %

 θ - ratio of inlet total temperature to standard temperature of 518.6°R

 ρ - mass density, lbs-sec²/ft⁴

 σ - solidity, ratio of chord to spacing

- total pressure loss coefficient (labelled OMEGA - B, Table 4)

 ω - angular velocity of rotor, radians/sec

Superscripts:

- relative to moving blades

designates blade metal angle

Subscripts:

ad - adiabatic

p - polytropic or profile

- r radial direction
- m meridional direction (in z-r plane)
- sh shock
- ss suction surface
- z axial direction
- θ tangential direction (labelled O, Table 4)
- 0 plenum chamber
- 7 instrument plane upstream of rotor
- 8 station at rotor leading edge
- 9 station at rotor trailing edge
- station at stator leading edge
- station at stator trailing edge
- instrument plane downstream of stator

APPENDIX 3

BLADE-ELEMENT AND OVERALL PERFORMANCE

Table 4 Identification of TablesTable 5 Design DataTables 6-9 Test Data

TABLE 4

			V°-2 SC FT/SEC	8 .y									
			V'-1 FT/SEC	, , ,	ν <i>θ</i> ·-2 FT/SEC	ν'θ9					-		
			M'-2	M'9	Vθ'-1 FT/SEC	ν'θ8					,		
	70		M:1	W,8	B'-2 DEGREE	6,8		STAGE PARAMETERS PT2/ TT2/	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		η_{ad}		
	EADING		U-2 FT/SEC		B'·1 DEGRÉE	88		TAGE PAR	P ₁₁	%EFF-P TOT-STG	$a_{\mathbf{p}}$		
	H NWOTO		U-1 FT/SEC	n ₈	%EFF-A TOT-ST	$\eta_{ m ad}$				H			٠.
	MANCE CO		.1 M-2	М8 М9	%EFF-P TOT-ST	ηp	//A1 :/SQ FT. 		M-1 M-2 M11 M10	%EFF-P STATIC-ST	ďμ	EFF.P INLET %	$\eta_{ m p}$
	IDENTIFICATION OF BLADE-ELEMENT OVERALL PERFORMANCE COLUMN HEADINGS		B-2 EGREE M-1	. 69 M	P PT2/ L PT1	P ₈	$\begin{array}{c} WCI/AI \\ LBM/SEC/SQ FT. \\ \hline \frac{w\sqrt{\theta}}{\delta A_{an}} \end{array}$		DEGREE N	-P PT2/ AL PT1	2 σ P ₁₀ P ₁₀	-AD ET	734
TABLE 4	OVERALL	·	B-1 B-2 DEGREE DEGREE	g,	A-B LOSS-P AL TOTAL	$\frac{\omega\cos\beta_9}{2\sigma}$	EFF-P INLET % \$\textit{\eta}_p		DEGREE \$10	OMEGA-B LOSS-P TOTAL TOTAL	$\frac{\overline{\omega}\cos\beta_{11}}{2\sigma}$	STAGE PARAMETERS EFF TO/TO PO/PO INI INLET INLET %	급
	LEMENT (Λθ9	OMEGA-B D-FAC TOTAL	13	EFF-AD INLET % η_{ad}	VØ-1 VØ-2	FT/SEC $V_{\theta 11}$	OMEC D-FAC TO	Ω	STAGE PA TO/TO INLET	耳
	BLADE-EI		. Vθ.1 Vθ.2 FT/SEC FT/SEC	ν 8θ		۵	PO/PO INLET Po Po			RHOVM-2 D-	ρ11V _{m11}	WCORR INLET LBM/SEC	$\theta \sim w$
	TION OF		VM-2 FT/SEC	V_{m9}	1 RHOVM-2	6m ^V e9	TO/TO PRINLET IN $\frac{T_9}{T_0}$	VM-2				NCORR WINLET I	
٠	NTIFICA	-	VM-i FT/SEC	V _{m8}	RHOVM-1	ρ8Vm8	SS III	V.W-1		RHOVM-1	ρ10V _{m10}	S Z Z	z
	IDE		V-2 FT/SEC	6	TURN DEGREE	9 7		V-2	FT/SEC	TURN	δΔ		
			V-I FT/SEC	^	DEV DEGREE	6,9		V-1	FT/SEC	DEV DEGREE	δ°11		
			EPSI-2 DEGREE	69	INCM DEGREE	im8		EPSI-2	DEGREE	INCM	ⁱ m10		
		~	EPSI-1 DEGREE	68	INCS DEGREE	. <mark>-1</mark>		OR EPSI-1	DEGREE F10	INCS	i _s 10		
	-	ROTOR	SPAN	- 95 to -	% SPAN	- 95 to -		STATOR	Span span	95 % SPAN	5 9 <u>5</u>		-

TABLE 5
BLADE ELEMENT AND OVERALL PERFORMANCE DESIGN DATA

FT/5LC 607.39 607.39 682.85 682.97 752.20 858.92 968.37 1045.08			
V:-2 FT/56 607.39 652.85 682.97 752.20 858.92 968.37 1045.08			######################################
F1/5EC 1044.7 1090.4 1136.6 1268.2 1268.2 1426.8 1568.1 1682.2 1708.1	N.,	112/ 111 111 1237 12302 12302 12303 12313 12316 12510 12510	
5218 5218 5607 5856 6405 77250 8880 8680 8644 8270	VB*-2 179.7 -179.7 -256.1 -317.0 -463.7 -638.5 -788.9 -885.9 -885.9 -886.0 -886.0	P 7.27 P 7.17 P 7.17 1.8655 1.9002 1.9242 1.9585 1.9466 1.9282 1.9158	#EFF-A TOT-STG 82.13 86.54 89.23 91.14 89.00 83.39 79.98 71.46 67.41
9653 9653 1.0087 1.1788 1.3308 1.4597 1.5864 1.5880	V8 * - 1 F 7 / 5 E C 844.1 -843.0 -945.5 -1077.8 -1244.7 -1397.6 -1505.9 -1539.2 -1571.0		•
z	B - 2 DE GREE. 17.22 23.11 27.67 38.07 48.03 54.56 57.97 59.09 61.51		
EC FT/SEC FT/SEC 1 987.5 0 988.3 0 988.3 1110.2 1 1736.5 6 1361.0 6 1361.0 1 153.8 2 143.8 2 143.8	6.89	- -	· · · · · · · · · · · · · · · · · · ·
F175E 844.1 844.1 893.0 941.5 1077.8 1244.7 1397.6 1505.9 1539.2	8EFF-A 101-51 DI 1015-51 DI 1015-		•
834 834 813 795 747 700 659 657 658	#EFF-P #EF 101-51 101 9276 9944 99414 99542 9515 9515 9515 9515 9720 88848 88 8848 88 8364 77941 77652 77552	# 2 250 550 578 588 588 588 588 588 588 588 588 588	FF-P 7666 8039 8311 8311 8311 876 8413 7985 7733 7733
569 579 579 590 621 651 655 640 631 633	_	н=1 .873 .858 .845 .812 .781 .767 .767	PT 2
DEGREE 53.29 53.29 50.65 49.26 47.57 46.15 45.34 45.34 45.70 47.74 45.70	PT2/ PT1 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	EE EE E E E E E E E E E E E E E E E E	
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u	DME GA - B 101AL 1157 1157 10931 1064 11514 1164 1377		OMEGA-8 TOTAL TOTAL 163 103 005 006 006 110 112 112 112 113
	D=FAC D 5936 5842 5837 5842 5837 5842 5831 5931 5931 5943	EFF P # C1/A1 INLETLEM 5 LC 8 9.8 42.04 89.8 42.04 89.8 7.5 EC 0 00 00 00 01 00 00 02 00 00 03 00 00 04 00 00 05 00 00 0	
9 L		VB: FT/5 752.3 711.0 684.5 638.2 597.1 579.0 580.7 600.8 648.8	RHOVM-1 RHOVM-2 D-FAC 5245 4641 4410 4410 4410 4410 4410 4410 4410
FT/SEC 580.18 660.49 664.91 592.25 574.46 551.56 554.34 537.71 493.36	7 - H > O + H = O + H		2
VH-1 F7/SEC 615.490 625.705 636.763 668.382 697.336 702.305 687.50 678.618 678.618		P D / P O INLET 2.0 2.0 2.0 4.75 C F F 7 S O 675 D G 675 D G 6	
V=2 770.440 946.940 926.804 877.741 829.215 801.681 793.611	TURN DEGREE 31.88 28.27 20.13 12.71 8.77 7.52 7.12 5.38	10,10 1NLET. 1,247 V-2 663,52 690,19 699,94 699,94 699,94 699,94 698,34 695,34 697,22 667,62 667,66	TURN DEGREE 48.10 45.74 44.41 44.40 39.75 39.75 44.40
V-1 17/3EC F 615/494 625.705 668.382 668.382 668.382 670.305 686.769 670.550	DE CREE 12.20 10.75 10.75 9.80 7.50 7.50 4.60 3.10 3.42 3.82 4.40	V-1 17/5EC F 1010:79 992.99 978.26 944.83 916.89 910.49	DEV DEGREE 11.80 11.05 11.05 11.25 13.40 15.43 17.00 18.90 MCORR INLET
* * * * * * * * * * * * * * * * * * *	JNCH 4.6S 4.72 4.70 4.46 4.03 3.70 3.45 3.45 3.32	51-2 645E	INCH OLGREE D 482 3.33 3.0 3.1 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2 3.2
EPS1-1 E	NCS 1.40 0.96 0.55 0.55 1.22 1.89 2.29 2.29	SI-1 EPSI-2	NCS 678 E D1 195 40 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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TABLE 6.1 BLADE ELEMENT AND OVERALL PERFORMANCE 50% of Design Speed

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M'-2 V 27704 3038 3738 3738 3739 3739 4310 4311 4421 4422	V82 FIXSEC -60.8 -113.5 -115.1 -241.1 -241.1 -401.6 -401.2 -401.2 -401.2	PT2/ PT1 1-2092 1-2092 1-1977 1-1978 1-1506 1-1506 1-1563 1-1563	#EEF-A 1701-510 85.13 90.97 91.62 87.77 82.77 82.77 83.17 63.17).
4492 4492 54992 55995 5692 7032 7211	A 81-1 1 DEGREE DEGREE 1/55-7 1 DEGREE DEGREE 1/55-6 9 63.55 18.88 -496.9 -66.68 3 36.55 -539.9 -7 2 66.68 3 36.55 -539.9 -7 7 72.18 58.24 -624.5 -7 1 74.47 65.66 -786.9 -7 1 74.47 65.66 -786.9 -7 1 74.47 65.66 -786.9 -7			."
17.55 4.78 4.93 4.93 5.59 6.79 6.79 7.74 7.74 7.55 6.55 6.79 7.74 6.55 6.55 6.79 7.74 6.55 6.79	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
U-1 1/SEC F 4422.6 4471.0 5539.9 654.0 7700.6 757.2 771.4	05 - 11 05 - 11 05 - 12 05 - 13 05 - 1		•	
μ	# EFF-7A 101-53 91-59 93-99 93-99 93-99 93-99 10-49 68-19 68-19	6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		
# 45551 44551 44551 44551 44554 4455	400 901 - 70 901 - 70 9	# - 2	77.0-1 71.0-1 71.0-1 67.5-3 67.5-3 70.04 70.68 59.52 57.41 55.63	,
H-1 -1951 -2023 -2023 -2092 -1092 -1962		Z 2224MMWW - mastannunu - mastannunun - mastannunun - mastannunun - mastannunun - mastannunun - mastannunun - mastannunun - mastannun - ma	P11 SIATC-SI 9063 71-76 9949 67-89 9949 67-89 9940 73-82 9900 73-82 9901 70-68 9901 70-68 9901 70-68	
9-2 0ECREE 48.2 48.2 46.2 46.2 45.3 91.11.	PT2/ PT1 1.2203 1.2203 1.2275 1.1954 1.1758 1.1758 1.1762		6	
D 0	1055.7 -0333 -0333 -035 -0145 -0277 -0377 -0378	00000000000000000000000000000000000000	1058 1018 1018 1018 1018 1018 1018	
2 B-1 55 C D C O C O C O C O C O C O C O C O C O	c)	7 7 9 2 2 2 2 2 2 3 3 4 4 4 4 4 4 4 4 4 4 4 4	THOUM-1 RHOW-Z D-FAC OMEGA-5 LOSS.P. TOTAL	
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FT/SEC 		V V V V V V V V V V V V V V V V V V V	114 85 25 25 25 25 25 25 25 25 25 25 25 25 25	
VM-Z FT/SEC 299-1 329-2 337-2 300-8 201-8 274-9 251-2 251-2 251-2 258-6 219-9	RHCVM-2 23.71 23.71 24.75 27.1	VH-2 433.8 423.6 423.6 410.6 310.6 310.9 311.2 290.9	1 RHO 34, 33, 34, 25, 25, 25, 27, 27, 27, 27, 27, 27, 27, 27, 27, 27	
VM-1 217.5C F 217.1 221.0 224.7 231.8 232.6 221.5 221.5 211.5 211.5	RHOVM-1 RHCVH-2 16.52 2.371 16.84 26.10 17.35 26.10 17.41 20.15 17.01 20.15 16.57 10.29 16.57 10.29 16.57 10.29 16.38 16.48 PO/PO EFF-AD	VM-1 77/SEC 341.0 341.0 370.2 370.3 272.9 272.9 272.9 272.9	26.86 29.09 29.09 29.09 26.14 23.28 21.55 21.55	PO/PO INLET 1.1749
V-2 17/5E F 513.6 503.6 485.2 392.7 376.0 356.3 356.3	DEGRET 51.23 44.63 49.45 49.45 113.85 113.85 113.85 113.85 113.75 113.85 113.85 113.85 113.75	V-2 434.9 424.6 424.6 371.4 3312.0 301.6 299.3	0	T0/T0 INLET 1.0601
V-1 1/SEC F 221-1 221-1 221-8 231-8 232-6 221-0 221-0 211-6	0 C C C C C C C C C C C C C C C C C C C	7 (2 (2 (2 (2 (2 (2 (2 (2 (2 (DEC 12,51 11,52 11,52 11,52 12,92 13,42 15,40 17,40	MCORR INLET LBH/SEC 74. 69
	14CM 050REE 13.58 13.58 12.74 12.74 12.53 11.54 11.54	10 10 10 10 10 10 10 10 10 10 10 10 10 1	DEGRES 1000 1000 1000 1000 1000 1000 1000 10	NCORP INLET RPM 1 5545.
EPSI-1 EPSI-2 DEGREE NESREE 15-181 12-374 15-329 10-185 2-592 -2-377 -12-635 -8821 -13-651-13-676 -17-518-13-676	INCS DEGREE 7.45 7.46 8.67 10.71 10.32 10.32 10.32	E 055.1.1 10.00 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	INCS 056REE 7.74 7.74 7.74 2.73 2.73 7.55 11.28 11.28	
7 % Span 5 % Span 10 110 115 115 115 115 115 115 115 115	% Span 5 10 10 10 10 10 10 10 10 10 10 10 10 10	R Span 5 Span 10 10 10 10 10 10 10 10 10 10 10 10 10	% Span 5 10 10 10 10 10 10 10 10 10 10 10 10 10	

TABLE 6.2
BLADE ELEMENT AND OVERALL PERFORMANCE
50% of Design Speed

ROTOR

50.0	•												•					
% Span	ME 48 ME 4	NW	# # # # # # # # # # # # # # # # # # #	NU-NC	A	18 /- 04 06 /4 07 07 07 07 07 07 07 07 07 07 07 07 07		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			200 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	N 50 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	100 00 00 100 100 100 100 100 100 100 1	DF 44 0 44 V V V V V V V V V V V V V V V V	1	2	- 14 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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			·	10/17	1.1785 1.1785	12 E 1	18 E T L	#C1/A1 A#/SEC SpFT 17,36					-					
97 ATOR 96 Span 96 Span 97 Spa	6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	N	> N N - N N O O O O O O O O O O O O O O O		>	L C C C C C C C C C C C C C C C C C C C	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	O FOR NOW A	E Q & & & & & & & & & & & & & & & & & &	The score of the s		- PMU				44.000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
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		TOUR TOUR TOUR TOUR TOUR TOUR TOUR TOUR	MCORR INLET AM/SEC 76.96	TO/TO INLET	PO/PO INLFT 1.167A	FFF-AD INIET 8 AO 19	INIET 8 80.56											

TABLE 6.3 BLADE ELEMENT AND OVERALL PERFORMANCE 50% of Design Speed

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FT./SEC TASEC TASEC TASEC TASEC TASEC FALC.4 4.12.4 4.12.4 4.12.4 4.12.4 5.50.9 5.50.9 5.50.9			77 13 13 15 15 15 15 15 15 15 15 15 15 15 15 15	
22.00.00.00.00.00.00.00.00.00.00.00.00.0		112/ 111 111 120519 130595 130695 130693 130524 130534 130535	ADEK-P. 1701-STG 85.92 92.62 93.32 93.32 95.95 85.95 85.95 85.95 85.95 85.95 85.95 85.95 85.95 85.95 85.95 85.95 85.95	
	N. image and and	•	57.5 2.13 2.13 2.13 2.13 2.13 2.13 2.13 2.13	
3106 3497 3668 3721 4245 4872 2003 5034	V82 EILSEC -132.3 -132.3 -132.3 -132.3 -265.0 -266.3 -501.7 -501.7 -513.5	PT2/ PT1 1.1946 1.1946 1.1713 1.1473 1.1477 1.1365 1.1366	AKER-A TOT-CYC 85.51 92.49 93.21 86.78 86.74 86.74 87.26 71.26 51.57	
46.02 46.02 46.02 5.398 5.596 5.721 7.7297	A 94-1 10 DEGREE EX/SEC.E. 15 59.78 12.26 -422.4 14 66.68 19.52 -446.6 14 66.88 19.52 -446.6 15 64.10 39.11 -539.7 15 64.10 39.11 -539.7 15 63.82 56.81 -710.8 17 71.50 61.20 -756.9 14 71.59 63.87 786.0	'.		
17.55 47.85 5.33 5.33 6.17 6.17 6.17 7.25 6.17 7.25 6.17 7.25 6.17 7.25 6.17 7.25 6.17 7.25 6.17 7.25 6.17 6.17 6.17 6.17 6.17 6.17 6.17 6.17	66 66 66 66 66 66 66 66 66 66 66 66 66		-, - ;	
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# =2 .4601 .4601 .3865 .3499 .3279 .3092 .3298	107.51 92.89 92.89 92.65 92.65 89.02 875.58 775.58		P72/ TEFF-P 9855 57.89 9858 57.89 9952 77.91 9956 82.77 9942 77.56 9928 74.18	
невроения	670 670 670 670 670 670 670		** C	
M-1 -2201 -2241 -2279 -2350 -2359 -2359 -2359	960884688 #F H		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
• • • • • • • • •	P12/ P11-2156 1-2156 1-2090 1-1016 1-1618 1-1437 1-1353	မျို့စုရုပ်သရုပ်မှုမှ		: •
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WO DO DO DO DO	LOSS-P 10781 10781 10781 10781 10782 1	19 N U W B N K S W F	NE did did did did	
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V8-2 401.3 351.2 354.4 298.9 2117.2 223.7 223.7 223.5	0MEGA- 1205 1205 1205 125 125 125 125 125 125 125 125 125 12	7.48 7.48 7.48 7.48 7.48 7.48 7.48 7.48	Ö	
22222222222222222222222222222222222222	. O . O . C . C . C . C . C . C . C . C	F,	7 A 7 A 7 A 7 A 7 A 7 A 7 A 7 A 7 A 7 A	EFF-P INLET * 84.04
္ကုပ္ထင္ မွာ		VE-1 VB-2 B-1 C FI/SC FI/SC DEGREE DE 0 390.6 - 34.0 40.5 0 325.6 - 32.2 33.5 2 285.9 - 22.1 38.0 2 219.2 - 25.1 35.4 0 219.2 - 25.1 35.4 0 219.2 - 25.4 0 215.2 - 27.4 0 215.2 - 27.4	RHOVH-1 RHOVH-2 D-FAC OMEGA-9 LOSS-P-101AL 101AL	F X 4 8
¥6-	Z	> F m m m m m m m m	221 221 231 38	AD ET 76
O T	PHOVM-1 RHOVM-2 18.26 26.95 18.56 29.34 13.87 25.95 19.86 21.43 19.69 19.94 19.59 19.94 19.59 18.62 18.59 18.62 18.59 18.62 18.59 18.62	VM-2 F1/SEC 4788.0 4788.0 4788.0 4788.0 461.0 411.2 3382.0 3382.0 338.0	2 2 3 3 4 4 5 6 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	EFF-AD INLET * 83.76
7.2 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3 7.3	26 22 25 25 25 25 25 25 25 25 25 25 25 25	445 475 475 475 475 475 475 333 333 323 320	ē .	Li
VM-2 541.7 541.7 341.7 373.7 373.7 307.3 200.4 270.3 252.1	1 9 7 7 7 9 0 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	ന അവരെ ആവരെ ആവരു ആ സ	7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	PO/PO INLET
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7. V-2 828. 817.85 817.4 8381.4 835.3 835.3 835.3 835.3 835.3	1088 41.15 41.15 36.64 11.05 11.05 11.05 6.77 11.05 11.05 11.05 11.05 11.05	3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	- magagement	•
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V-1 77/SEC 244.6 254.6 251.2 251.3 258.7 258.7 258.7 259.8	DEV 64EE 3.30 3.30 3.30 3.24 7.71 5.95 6.33 7.46	7 K 2 K 2 K 2 K 2 K 2 K 2 K 2 K 2 K 2 K	112. 112. 112. 112. 113.	P S S S S S S S S S S S S S S S S S S S
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E 051-1 E PSI-2 D 578E D 56RE E 15.734 12.996 13.05 12.996 10.25 10.002 2.838 4.934 -5.019 -1.754 -11.955 -8.216 -11.951-12.957 -17.222-14.103	7	E e SI - 1 D E G R E E 113.939 112.101 110.697 5.922 5.922 - 1.420 - 1.420 - 1.420 - 1.420 - 1.420 - 1.420		
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86	· .	ec &	1 8	

ROTOR

TABLE 6.4
BLADE ELEMENT AND OVERALL PERFORMANCE
50% of Design Speed

TABLE 6.5	BLADE ELEMENT AND OVERALL PERFORMANCE	50% of Design Speed

FT/SEC DEGREE DEGREE 315.2 3	ROTOR 8 Span	1-1563	EPSI-2			1- H-1	. 2-E	v 43-1	30% U.		gn opr 8-2	D	Į.	3		7		· ·	, ,
10 1.075 1.085 102.5	~ <u>e</u>	15.709	066REE 15.280	283.0	4	7/SEC F 283.0	7/SEC F1	1/SEC F.	7/SEC DE		685 43.6		5055	FT/SEC *25.C	FT/SEC	-	- 1		- (
Second Color Seco	. z s	10.257	10.835	292.9		292.9	428.5		315.2				4749	449.4	4 36 .5 512.1				
No. 11-162 1-102	38	-5.120	-1-783	304.7		304.7	365.2		254.9				4143	542.9	558.7				
Second Color Seco	2 3	-11.812	-8.092	2 99, 7		299.7	345.9		160.7				1396	7.00.0	620.9				
State Color Colo	28	-16.432	12.748	292.6		292.6	330.0		199.4				3235	161	729.7	İ	- 1		- 1
The color Color	. x	-17.675	15.135	289.0		2882	275.6		143.7				2756	7.00.7	745.2		i		
1.00	% Spen	TNCS	INCH	A20	TURN	RHOVM-1			04EGA-3		PT 2						1 VB*.	-2	
1, 4, 1, 7, 5, 11, 11, 2, 5, 11, 11, 11, 11, 11, 11, 11, 11, 11,		75	7.19	11.92	1 C C C C C C C C C C C C C C C C C C C	9			T 07 AL	-	*		_	ST DEBR	EE. DEGRE	E: F1/5E	C ETZSE		
15 1-4 7 7-51 1-65 10 1-65 22-65 10-12 11-	. 2	1.08	7.51	12, 63	38.23	21.33	23.75		1451		•			28 56	19 12.	09 -425	-88	.	
25 2 1 5 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2	2.43	7.51	11.88	33.52	21.63	33.21		9110					56 57	13 18	85 -449.	3 -149.	on	
5.55 6.76 6.76 5.27 10.17 27.12 27.19 10.07 11.19 11.12 5.0.18 5.56 6.75 6.7. 6.2. 6.3. 7.70. 6.2. 6.3. 7.70. 6.2. 6.3. 7.70. 6.2. 6.3. 7.70. 6.2. 6.3. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7.2. 7	R 5	2.81	7.22	9.06	22.87	22.26	30-17		.3682					25 60.	92 37	95 -5 42	9 -303		
5.5.5 6.76 6.76 5.20 0.87 21.62 23.8 .2506 .1100 .0113 1.0913 96.51 96.59 65.96 65.00 77 65.10 1.0013 96.51 6.61 6.76 6.20 6.96 21.48 22.8 .2506 .1101 .0118 1.0719 96.51 66.99 65.90 65.9		5.58	7.41	2.4.2	10.71	22.10	26.19		0.070					75 64	17 48-1	77 -627	5 -417.6		
Second Color Seco		e 10 · 10 · 10	6.76	5.20	8.83	21.62	25.48		.0729					37 68.	90 67-1	347 LYa	4 - 5 0 5.	<u>.</u>	
Separate Separate	3 %	5.71	5.61	6.95 8.73	4.27	21.48	23.18		1100					96 69	166 63.5	10 -775	7 -500-5		
Span EFSI-1 FPSI-2 V-1 V-2 VH-2 VH-3 VH-2 VH-3 VH-2 VH-3 VH-2 VH-3 VH-2 VH-3 VH-2 VH-3					T0/T0 IMLET	PO/PO INLET	EFF-AD INLET	EFF-P INLETL	WEI/A1 BH /SEC						•				
Span DEGREE DEGREE FLYSEC FLYSEC FLYSEC DEGREE DEG					1.0423			87.88	21.60										
Span SPAIL	~5			•				•		٠					•				
5 19.025 9.559 601.5. 599.2 466.0 587.8 580.2 1.02		EPSI-1	FPSI-2	V-1	-		VH-2 1	V6-1	V8-2		2-8	7	2-k					112/	
12.25 3.61 6.91.0 532.1 866.7 530.7 335.3 -40.5 34.8 -15.9 5.95 5.95 5.95 1.172 1.1. 15. 10.713 3.684 566.7 565.1 366.8 3.22 3.24 -40.5 5.94 -40.5 5.95 1.172 1.1. 20. 5.319 4.56.8 513.0 431.4 513.7 523.1 -40.5 3.482 -40.5	~	14.025	4.554	601.5	٠		587.8	380.7	ร	š	5 K F F		4264					171	
10 1.1.7.2 1.1.7.2 1.1.2 1.1.2 1	2:	12-235	4.156	591.0			583.7	335.3					5213					1.0544	
1.2 1.2	2 8	10.77	3.80	567.7			562-1	306.8					5045			-		1.0515	
70 -1.56 9 573 835.9 928.1 808.7 927.0 151.9 -25.9 21.8 -40. 3899 3823 1.1077 1.2 81	8	2.139	1.448	169.0			311.7 466.8	253.1					4587					1.0454	
Spin DEGREE DEGREE DEGREE DEGREE DEGREE DEGREE STATES 175.2 120.3 %.C 3318 1.000 1.0	٤;	-1.769	.573	135.9			427.0	151.9					,3823					1.0348	
Spin OFGRE DEGREE DEGREE STATE S	2 8	765.4		425.5			393.6	197.4					3518		-			1,0340	-
SHAN DEGREE DEGREE DEGREE DEGREE DEGREE TOTAL TO	2 %		549	393.0			348-2	117.9		22.2			3339			_		1.0347	
-2.89 C.3 12.51 % S.5.7 % S.66 190% C.5	% Span	INCS	INCH	DEV	TURN	RHOVM-1				LOSS-P		# E F F	ا				SET .		4.
-6.59 -3.55 11.52 38.75 37.04 43.57 1690 .0255 .3927462246 89.48 89.48 -1.55 11.52 10.92 56.48 10.25 11.52 10.92 56.48 10.25 11.52 10.92 56.48 10.25 11.52 10.25 11.52 10.25 11.52 10.25 11.55 1		-2.89		12.51		15.17						SINIC	5.		. *		S I		2 :
-7.56 -4.62 10.92 56.84 56.83 82.33 .1600 .0228 .0216 .98673302.93 90.24	9	-6.59	- 3, 55	11, 52	38.75	37.04						7-472.0	9		•		9		2.2
-[5.7] -5.5 14.6 25.49 31.61 35.45 41.5 41.5 41.6 31.60 4.95 31.6.14 4.5 41.5 41.5 41.6 41.6 41.6 41.6 41.6 41.6 41.6 41.6	 	7.56	29.4	10.92	36.84	36.43						73302.9	5				90.2		ည္
-13.65 -10.52 13.45 25.87 30.76 32.49 .159.9 .00.9 .9958 2.42 .29.2 .9 .9 .25.5 .9 .29.5 .9 .	2 8	4 6 6 1	70.0	17. 73	20.00	23,05						2 171	9.				9.08		2.5
-15.19 -11.61 15.89 24.32 30.20 29.78 .02108 .0286 .9923 30.10 71.88 62.83 -11.84 17.80 25.35 28.58 28.22 .2274 .0781 .0263 .9936 50.43 62.83 62.83 62.83 -11.85 62.83 62.83 62.83 62.83 62.83 63.29 62.83 63.29	2	-13-85	-10.52	13, 45	28.82	33.78						7. 2. 4 B	24				82,9		7.2
-13-65 -10-27 19-68 26-23 27-28 26-17 -2582 -1165 -00-19 -3906 46-43 53-24 53.24	£ &	-15-19	-11.87	15,89	24.32	30.20						3 38.1	91			_	71.4		2
	8	-1 3- 65	-13-21	13.68	26.23	27.28						46.4	2 2				53.2		58

MCGRR WCGRR TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET INLET INLET INLET RPM LBM/SEC 1.0423 1.3278 82.73 82.93

TABLE 7.1 BLADE ELEMENT AND OVERALL PERFORMANCE 70% of Design Speed

	F 25588						•				•	•	•			_			
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		DEGREE	DEGNEE	FT/SEC F	•	•		/SEC	õ	REE DEG			•	-			•	13EC	1/5E¢
		15.750	15,306	131.4				•		20	•	•						79.5	438.3
The color of the		10001	13.02V	337.6			467.9			•	•	•						712.2	2000
Size Size			70.0								•	•						0.67	
		15.602	2005				5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7			•	•	•						7.000	
State Colored Colore											•	•							
		-14.779	1 2 4 2 2								•	•	•	•					
State		17.070	4.077	337.7			0 - 1				•	•						24.0	70
		-17.490-	15.093	335.6			5.001					•	• -					153.4	7.6.6
State Colore Co		•									'	•	•						
Second Colored Color	ì	SUN	_	O.E.v	200	1 - N - O - O - O - O - O - O - O - O - O	20.00	1	_	0.00	012,	9 - 7 - 7	46.6.4		4	1 - 6 - 6 ×			
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	% Span		DE GREEF				7114514	,		10101		10101	101	FGREE	DE GREE	67/56	77/56		
10 10 10 10 10 10 10 10	•	5.25	11.48		47.0	34.34	15. 24	55.60		9160	0 7 9 7			60.67	12.76	593.2			
1,	n <u>s</u>	5.47	_	14.36	0	24.46	9 - 0			9000	1.462	6	9 9 9	61.53	20.58	-627.1	177.0		
Second Color Seco	2 2	5,72	_	13.21	36.48	25.05	40.0	4602		9500.	0757	101.77	101.90	62.36	25.87	-661.1	-231.9		
State Stat	2 \$	6.82	_	4.83	25.11	25.78	35,31	5012		• 6 1 0 •	1.4019	93,88	93.61	64,83	39.72	-757.8	-347.3		
10 10 10 10 10 10 10 10	3 5	6,30	_	9.10	16.37	25.90	32.19	4837		.0211	1.3688	17.54	87.01	67.92	51.55	-875.4	-478.7		
State Stat	6	60.6	-	6.32	13,39	25.41	31.07	1718		.020	1,3672	7.10	80,32	70,57	57.17	-983.3	-572.9		
99 9,83 9,90 6,86 9,74 2746 24,50 15073 1513 10024 1,3866 6,75 66,14 72,00 4,71 170,70	\$6	8,83	-	6.25	11.07	24.81	27,71	5044		.040	1.3695	72.03	70.79	72.19	61.12-	1062.8	-612.3		
10,70 10,7	8	6,63		4.86	4. 7	24.66	26.50	5093		-0424	1.3686	69.7B	****	72.66	42.90-	1082.7	-629.5		
Sum PES_1-1 PES_1-2 PES_1-2 PES_2-3	\$6	9 . 8		7.48	9.16	24.53	26.07	5103		• 0429	1,3051	67.79	* 6 . 3 4	73.07	-14.49	1103.7	-650.6		
									*										
Sun Effect File					10,10	9/0	Ė	d- j.3	#C1/A1										
Sum EPS -1 EPS -2 V-1 V-2 V-1 V-2					INLET	Ä	Ē	INLETL	BM/SEC										
Sum					•	:	•	-	5067										
Spin EPSI-1 EPSI-2 V-1 V-2 VH-1 VH-2					1.170	1.3935	90.00	92.6	74.7										
SAM PESS EPSI-1 EPSI-2 V-1 V-2	ATOR													-					
		EPS1-1	EPS1-2	-			VH-2			1.8	-		~			•		112/	
\$ 13.447 9.550 740.5 596.2 696.8 64.9 64.0 6.9 49.0 5.0 6.31 6.651 15 10.627 3.491 70.6 561.6 524.7 560.9 470.7 6.1 44.0 5.0 6.316 6.665 30 7.407 3.129 6.32.9 560.9 470.0 6.2 6.2 6.2 6.2 6.2 6.2 6.2 6.2 6.2 6.2	2	DEGREE	DEGREE	FT/SEC.	T/SEC F	T/SEC F	T/SEC F1	•	ĕ	GHEE DI			1	÷		_		Ξ	
10 12.19	•	13.947	4.550	740.2		488.8	594.9			0.6		•	189			-		1.1237	
15 10 + 627 3 + 94 1 70 + 6 + 6 1 4 + 1 4 + 1 4 + 1 4 + 1 4 + 1 5 5 5 1 1 1 1 1 1	01	2.147	4.206	722.8		522.2	580.4					•	150	-		-		1 . 1 1 3 6	
30 7-407 3-127 6-33-17 6-33-17 6-33-17 4-4-2 -550-3 -4-25 -555-3 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -5-25 -4-25 -4-25 -5-25 -4-25	15	10.827	3.941	704.		524.4	560.9					•	988			-		1.1107	
\$6	30	7.407	3.12	633.4		464.3	508.3					•	526			<u>.</u>			
## Span INCS INCH DEV TURN RHOVN-1 RHOVN-2 DEAG STATE	S i	10.1	90.7	585.5		200	7000		:			•	022			-		940	
90 -5.067 7710 562.0 932.1 901.8 932.0 920.9 -10.5 96.9 -11.0 90.0 3.576 11.2355 11.23555 11.2355 11.2355 11.2355 11.2355 11.2355 11.2355 11.2355 11.	2 8	7.00		582.7			2000					•	97.			: -		330	
95 -6-349 .700 577, 420.9 393.0 920.8 423.4 -8.3 47.3 -1.1 .499.3.3576 1.3267 1. 1859m	8 8	5.067	.710	562.0		401.0	132.0					•	478			-		1 . 1 3 7 3	
Span INCS INCM DEV TURN RHOVN- RHOVN- PLACE DFAC DFECA'B LOSS-P PT2/ REF-P FACT-ST DFAC DFA	8	**	. 700	577.7		393.0	420.8					•	574			=		70 1 1	
\$\text{Spin}\$ \text{DEGREE} \t		2	1	3	10:1	2	2	,	OWEGAL	-	017/						KRPP-A		
\$ 0.56 0.40 22.39 93.06 39.75 50.50 .1179 .0222 .9709 70.39 65.62 10 2.61 5.54 16.07 93.04 93.06 49.95 .3442 .3346 .3346 .3462 11 1.64 46.0 11.97 93.01 93.55 90.31 93.46 .3949 .75.59 12 1.66 46.0 11.97 93.01 93.06 93.90 90.70 90.75	% Span	2000	-		1000				TOTAL	•	-		-				TOT		
10 2.61 5.54 16.07 43.40 43.08 49.83 3.842 41313 5.034 5.687 67.54 6		40.0		22.39	43.08	39.75	50.50	3509	1179		970		٠.				65.62		
	. 5	2.61		16.07	3.40	43.08	40.83	3642	.1313								92.04		
30 3.88 6.87 10.35 47.20 39.08 43.90 4005 50877 50.25 7559 86-6-6 50 474 6.07 10.84 44.77 36-28 40.02 10.19 70 700 84.34 70 6.07 10.84 46.77 36-28 40.02 10.19 70 70 0 84.34 85 972 13.24 17.40 47.72 33.46 37.03 50.65 50.65 71.15	12	99.1		11.97	15.01	43.55		3836	1380								92.35		_
50 4°94 8.07 10.84 46.79 36.28 40.02 42.59 0.0421 40.90 89.00 89.34 70 4.04 9.28 12.70 4.74 35.70 36.42 45.63 .06.31 47.8 40.23 85 9.29 13.24 17.40 9.74 35.72 36.29 45.34 47.8 77.8 77.8 77.8 77.8 77.8 77.8 77.	8	9		10.35	47.20	39.08	43.40	4005	.0877								19:4		_
70	20	7 A .		.0.	46.79	36.28	40.02	4254	.0621								0.0		
90 10,44 14,17 20,01 47,64 3272 36,29 6514 6153 0545 9759 68,55 62,80 62,80 95 11,42 14,80 22,55 48,43 31,91 36,29 6514 61721 0621 9733 66,09 60,35 60,09 MCORR 10/TO PO/PO EFF-P FF-P INCET INC	0.3	*	•	7.0	9 7	35.70	69.67	454									7 6 7		
95		18.01	-	20-01		32.72	36.29	6214	. 1532								62.80		_
CORR &CORR TO/TO PO/PO "EFF-AD E THET INLET INLET INLET IN RPH LBM/SEC 5 7783. 11079 1.3464 79.78 4		11.42	-	22.55	48.43	16.11	38.21	9149	1721								40.38		_
NLET INLET INLET INLET INLET INLET IN RPH LBM/SEC S 7783. 110-43 1-1170 1-3664 79-76 4			890	8000	10.10	04/04		•	i										
LBM/SEC 5 1-1170 1-3664 79.78 1			NLET	INLET	INLET	INLET													
110-43 1-1170 1-3664 79.78 4			_	BH/SEC			-												
			٠.	110.43	1.1170	1.3664	79.78	-											

TABLE 7.2 BLADE ELEMENT AND OVERALL PERFORMANCE 70% of Design Speed

ROTOR * Span	EPSI-1				VH-1	V 5-NV	. 1-8,				# *	H-7		1-2	1747	H*2	٧٠-1	
<u>'</u>	DEGREE	DEGREE DEGREE F	T/SEC F	77.SEC F	1/SEC F		FT/SEC FT	FT/SEC 0E	GREE DE	SREE			٠,	FT/SEC		100	FT/S'C FT/SEC	FT./SE
ء م 	13.141	13.072			301.8	120.7	, -	172.7				6216		F 80.F	4053	47.7.4	7.9.5	101
2 2	10.383	10.882			347.8	478.2		7.16			3145	6054	667.4	721.5	6806	4642	752.6	528
8	2.727	8			359.6	472.7	.	8.44		٠	•	5353	7.55 .0	787+3	- +7649	4751	845.1	544.1
- S	-5.532	-2.027			361.9	390.2	0	9. +0		•	Ť	. 4883	894.2	8 14.9	.8646	.5309	955.	£11.
20	-12.189	750.8-			354.2	354.6	n •	93.1		•	•	16 31	9.2.6	362.5	.9534	.5841	.5841 1053.9	£76.2
S	-16 902-	17/97			7.000	1275	7 .	9.011		•	÷	1	5 7 7 8	7020	1810		77.	
8 8	-17.385-15.317	15.317	340,9	510. F	0 * O * E	308.1	, 0	407.1		• •		4354	1114.1	1572.0	1.0532	.6263 116	1165.1	732.8
			•														1	
	200		2	1001	1 47070	- A MORG		4						;	,	Š		
# Span		DECREE	EGREE		T. HAON	7-12	4	C OMERSA-B	1014	P 1 2 /	101-01	7 101-51		2-18		7-84	7	
•		17.61	12.27	48.15	74.51	35.40			10.0		•			12	15 90 9	3		
9		11.84	13.41	41.84	24.93	38 .87		.0298	0005	1.4747	7 - 98.24	- EG -		7 19.6	1 -6 33. 1	-167.		
2 2	5.66	11.74	12.32	37.31	25.13	40.36	4710	0138	0200-			100.05	52.10	2 4 5	24.00.057.4	-224		
S		10.80	90.6	25.76	26.10	35.84	.5088	2070	.0148					48. 4	A -765.0	-342		
S 59		10.84	7.93	17.51	26.24	33,17	£ 767°	1137	.0222			3 87.07	17 67.81	50.4	1 -R84 -2	-470.3		
2 8	8	10.83	6. 38	13,25	25.75	30.92	485.	15.70	0299		•		i	57.2	3 - 200 - 5	4.695		
8	8.11	36.6	6.37	10.8	25.16	27,96	.5059	.2278	00400		77.77		3 72.07	7 61.2	61.24-1072.9 -617.7	-617.7		
8		9, 78	6.9	9.56	25.02	27 -03	.5036	. 2391	4040					62.9	62,98-2093.0	# D#9-		
8	8.15	-9.65	7.91	8.12	24.88	25.90	.4997	.2493	.0402	1.3762	2 69.67			1	64.84-1114.1			,
			٠.															
			,	10/10	P0/P0	EFF-AD	EFF-P	MC1/ A1									1	
				INLET	INLET	1 E E	INLETL	BM/SEC										
				1-1210	1.4089	85 .05	85.73	85-73 25-23										
							1											,
STATOR	ì	_		;	;			•				;					į	
% Speri	11771	7-75-7	1-1	7-1	7 4 4 5 F F F	7-68		7-8-5 7-7-7-7-1	8-1			N + 1		-		P T2/	71.5	
•	1 1 912	405.44	787.9	•		F 1736.1	756	175E C UE	2 F 64	. O. E. E.	66.73	3663.				1		
9	12.647	4 - 12 3	733.2		520.9	586.7	515.9	0				.5110				1.0 779	2	
~	10.671	3.826	716.9	•	528.4	569.3	9.484	-39.7		2		4989				1.0741	1150	
8	7-173	2.949	546.5		475.4	516.1	438.1	-36.C		0.47					7.7	1.3936	1	
8	2.930	1.885	601.4		446.0	473.0	463.3	-33.1				.4041				1.3702	1,1178	
2 5	- 985	1 -034	584.8	452.6		5.154	396.8	-31.6		0.		- 38 B.F				1.3581	1.1216	
8 8	-4-111	6534	587.0	492.2	111.1	401-1	0.514	-30.8	. S. 6	0 0	5.58	1769			,	180	8	
 S &	-6.480	999	579.4	1.24.1	1004	123.1	419.0	-26.5		2 0		. 3604				1.3391	1.1971	
			,													,		
	INCS	INCH	DEV		R HOVM - 1	2-H AOH d 1	2 D-FAC	0			* * EFF	4		-		A-FOR	A SEPT-P	بە
E C	DEGREE	DEC RE	OEGREE	9							STA TC	-51				TOI-S		g
~ :	# 0 #0 #0 #	9. 5	12.51	53.23	39,95	51 53	•3836		.0250		75.	~ ;				86.26	80.91	= (
2 :	2-24	2.2	10.97		67.93						71	Q :				91.6		n :
2 8	4.29	7.29	11.25		39.67				.0238		15 78.	92				88.5	1	2
 &	5+45	8.59	12.03		37.27	40.99					3 79.	23				82.8	3 83.54	*
0,	7.06	10.29	13.45		35.69						34 76a	;				15.1		d d
- 8	10-11	13.43	15.89		33.78		٠		·		.2 69.	67				90.04		
8 8	10.47	13.80	17.40	50.07	33.29	36.62	.5308	.1573	.0558	1378.	51 67.57	57				63,98	65.42	~:
? 						•	•		•		:	<u>.</u>				1470	İ	1
	1	NC ORR	WCORR.	10/10	P0/P0						·							
		INLET	INLET	INLET	INLET	INLET	INLET											
		7857	111.86	1.1215	1.3803	7	•											

TABLE 7.3 BLADE ELEMENT AND OVERALL PERFORMANCE 70% of Design Speed

								0 0 0	or pesign	ığı Vode iği	t							
ROTOR % Span	EPSI-1	EPSI-1 EPSI-2	V-1 FT/560	Y-7	VH-1	VH-2 1	_	VB-2	8-1 9	8-2 K-1	1 11-2	2 0-1	0-2	11.8	1 N·-2		V1 V	
w i	15-755	15,339	371.5	739.1	371.5	481.9	_	9.09	5		1		•			361. 2	•	9
2 2	13.098	13.095	378.6	725.1	378.6	517.7		۲۰۰۷			•				-	863 7		50.1
: R	2.929	5.122	398.2	616.8	398.2	9.55.4		14.5			•					144 8		86.6
9	-4.771	-1.507	402.3	558.5	402.3	427.8		559.0								823 9		56.2
2 %	-11.311 -7	-7.778	396.8	533.4	396.8	0.074		28.9			•	•				586 100		N I
.	-16-941-	1.861	385.0	504.1	387.6	471.0		32.4			•	7.			,	7 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6		9 9
\$	-17.475-15	010	382.6	487.5	382.E	344.4		45.1		4.7 .3467	67 .4202	N2 11C7.			1.0618 .58	.6884 11.		7.867
% Span	INCS	INCH		3	RHOV#-1	RHC W-2	D-FA:	ONEGA-B		12:d	45FF-P	REFF-A	31 B	B 2 V	VB 1	1 . VB 2		
. *	DEGREE	DE GREE	-	-	36			TOTAL	TOTAL	P.11	101-51	4	CREECE	CAEE ET	ET/SEC. ET.	35.	:	
. 2	2.73				27.32		4249	8600	1,0021	1000	100.71		1 62.4	5- 58-6 8-80 -6	29.5 -1.	87.7		
15	3.03	٠		34.73	27.74	43.35	.4098	0358	0078	1.4494	102.58		9.67 2	9- 26-4	63.4 -2	4 4 7		
2	4.27	•			28.55		• 4566	.0680	.0143	1.3820	93.32		2.27 3	8.8 -7	60.4 -3	68.1		
8 5	5.83 5.83				28.81		. 4273	.0839	-0174	1.3408	89-07		5.65	0.03 -8	78.9 -5	10.7		
38	4.5				27.89		1007	1000	0510	1.4268	78.45				4	7 0		
8	6.63				27.73		4168	1875	0110	1.3167	73.08		9 94.0	1.77-10	86.5 - 7	02.5		
98	4.71			6. 77	27.67	29.27	.4265	-2162	.0358	1 - 3089	68.93	67.77	70.92 6	64-15-1107.5	07.5 -7	20.6		
				10/10	PO/PO	FFF-AD	4- 113	WC 1 / A 1										
				INLET	INLET	INLET	INLET	BH/SEC										
	-			1.1056	1.16.77		æ	27.77										
													-					
STATOR			•	5	3	,						٠,			į		;	
% Spen		7-15-1	1-A 67/56	67 /55	1 - WA .	7-44	7 4757 5	-		1-K 2-5	7	×			714		<u> </u>	
ν,	13,977	4.522	774.6	676.0	552.5	674.3	542.9		2	4	853 . 59				1-8175		12:12	
9	12-167	4.146	761.8	659 . 2	581.7	9. 159	491.9			•					7.47		11:22	
S 2	10.784	3.835	742.3	639.5	582.0	638.0	. L. 09.			•		60			1.40		1037	
R 5	7.056	2.8 55	661.7	583.8	520.7	582.3	K03.2			•		3 (0			97.		901	
2 5	2.298	1.625	611.5	538.5	7 . 25 e	0.00	357.0E			•					1.54		7.01	
. 2 6	455	100	597.5	8-064	1937.7	9 6 8 4	9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6			• •		14			1.10		5001	
8	-5.358	.512	5.88.6	473.7	473.2	472.5	350.0	-33.0	36.6	-4.0 .51	5123 .4084				1.2939		1.1151	
8	-6.469	.595	579.9	451.1	4.58.5	705	355.0			٠		78			1.27		11 32	
		:																
A C.	INCS		V30		RHOVM-1	1 RM0 VM-2	2 D-FA:	OMEGA-B	_		\$££ F.Jp					AEE-A	SEFF-P	
indo x	DEGREE		DE GREE	CEGREE					TOTAL		TATC-ST				¥ •		TOI-SIG	*
9	56.3 5.83		11.52						0116		67.58 87.58				o		4	
22	-1+89		10.92						0322		58-22				i 07		1	
33	28		11.25						.0133		80.74				•		90.32	
S 8	38		12.03						9,00.		89.69				œ ·		67.57	
0.88	12.4		15.89			12.12	13462		4 5		77.23				4 ~		13.2	
8	10-1		17.60	•					48.0		71.69				ع د		67.65	
	2-05	5.42	19.68	41.92	36.28	36.56		1071	-050	9778	67-45				ٻ ∙		6 3.06	
									**									
		MCORE	HCORR	10/10	P0/P0	EFF-AD							1	•				
		<u>.</u>	INCET	٦.	INLET		INLET											
		7811.	123-11	1.1066	1.30 76	•	•											

TABLE 7.4 BLADE ELEMENT AND OVERALL PERFORMANCE 70% of Design Speed

HOTOR	EPS1-1 E	2-154	;	٧-2	7		7	2-5	1-6	٠				;	-		-	
Linds of	NF COFF D			•	•	•		1		:	:							
~					-	•	,		GREE UE			-		110	,		73671	26/1
· :	15.753	1.00	2.7			487.5		1.56		Ī				64.0	• 6326	0.7.7.	698.5	200
=	13.090	3.1.7	378.8			9.405		20.9		•				90.9	.6423	.4697	731.0	632.
	10.406	0.980	385.4			A . 7 . 8		74.8						*	4920	900	743.6	547
\$			900							-				7 .				
\$?		•				6		. 5 Z 3 3	2.460	
-								0		•				0.5	97/8	.5.07	761.7	
2 :	- 5/4-11-	7/8.	74.5			*20.5				•				50.5	. 4543	. 6634	057.4	9
2	-10.165-1	2,584	387.4			401.2		19.2		•		_		15.4	1.0227	6985	128.2	803
8	-17.060-1	3.941	385.0			371.1		29.0				-		37.0	1.0387	41.69	46.0	798
86	-17.547-15.0	5.059	382.6	478.6	382.6	342.1		334.7			1967	1130	100.3	1050.7	1.0556		6.1911	600.7
_								•				•		• -	<u>.</u>		•	
-																		
	INCS	# J C #	DEV	T URN	RHOVA	RHOVH	P D-FAC	OMEGA-B	_		\$ EFF-	SEFF-A	 9	2		. 782		
min e	DEGREE D	REE	BEGREE	DEGREE				10741	TOTAL	٠	Total	107-51	DF GREF	DEGREE	FTISEC	FILSE		
,	2 27	70	12.91		94.46			0		•		1 1	67.79				,	
		:								-								
≘ :			97.71	-	27.33		-	• 0 3 6 8	.000	_	97.6	47.53	58.6	18.50	-629.2	-02-		
5		. 0		35,05	27,75		_	0112	4.0025	_	100.84	100.92	57,50	54.45	1.459-	-235.8		
8	-	9 . 6	9.21	22.99	28.58		•	.0510	.0107	_	94.85	94.65	62.09	39.11	-755.5	-376.2		
S	L	8.31	7.60	15.30	28.85					-		9.00	45.24		-A73.2	4.419		
2 5							-			•								
2 8		9		11.78	28.48		-	•0434	.017	-	86,32	85.8	68.02	56.24	-980-3	-633.5		
3 8		19.	•	10.24	27.89		-	504 -	.0260	_	78.87	78.07	6.4.9	59.5	1059.5	-6969-		
⊋ :		7.59	5.89	6.43	27.72		-	.1836	.0321	_	72.84	71.84	70,35	61.92	1079.4	-707-1		
56	9.00	7.50	7.48	. 40	17.57	27.93	181	.2156	.0353	1.2930	68.17	67.03	10.07	-1+0+9	1100.3	-724.0		
				•		•												
				10/10	04/04	EFF - AD	EFF.	#C1/A1										
				INLET	INLET	NET	NLET	BM/SEC						-				
_						-		SQFT						-				
				1.1031	1 - 35 - 8	89.42	88.88	27.79										
. actars							,									•		
	9 11.965					•									•			
% Span				7-7				7-1		×	Ŧ	~			•	P12/	112/	
	U GREE	-		-	-	•	_	/SEC DE	8EE 06		,						E	
۰	0.00		774.5					45.2	7.	•	•	596			-	Τ	.1193	
2	12.170		762.1					. 2.9.	1.7	_	•	937		,	-		1142	
15	10.712		740.4					40.6	0.0	•	•	4.8		-	•	_	1082	
8	980.9		658.0					64.7			•	401			-	_	000	
98	2.160									•	•	707			-	-		
2 5										-	٠.	90.			: .			
										•	٠	/20		-	•	_		
3 8	4574		1000						•	•	•	272			•	_	* 104	
2 2	0/216	. 524		9.57	473.0	0.87	338.3	- 53.1	5.7	-2.8	. 6073	0.1.		-	-	1 . 2 8 0 8 1	9011	
2			21776					•	7.5	•	•	*		-	:	_	• • • • • • • • • • • • • • • • • • • •	
			-	_														
× 6-22	SON!	ž	0£ v	T URN	RHOVM	RHOVEL	D-FAC	OMEGALA		PT 2 /	-			-		AEPT-A		ŀ
indo e	DEGREE D	EGREE	DEGREE	DEGREE	•			TOTAL	_	-	-	-				TOT-SIG		r.
•	1.87	. 7	20.20	40.58	44.18	54.92	.2734	.1216		.9673						85.40		_
0	֡֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	-	14.90	42.27	45.75	54.25	2907	1350		9646				_		98.54		_
~	4.4.	_	11.31	12.51	44.44	6.8	2	9111						-		17.11		_
: 5	7	-	9.77															
3 5	2.08	-				2	7007	100		4 2 4				-				
۶			11.77	70.	0					7.00								_
\$6	56.1-	1	15.29	38.15	39.37					86						72.69		_
8		-	18.41		,									_		1		_
8	1.29		22.80	30.05	35.96	36.36	97	1375	9440	4787	99.99		•			-	62.04	_
							•			•				,				
														-				
	Ź.	Œ	#CORP	10/10	P0/P0	EFF-A0	EFF-P											
	<u>-</u>		INLET	INLET	INLET	INLET	INLET											
		3	M/SEC	•		•	.											
		:	23.10	1.1031	1.3366	63.90	84.5							-				
														•				

TABLE 7.5
BLADE ELEMENT AND OVERALL PERFORMANCE 70% of Design Speed

1004000000 100400000 100400000			0 480MF
100 00 00 00 00 00 00 00 00 00 00 00 00		1112/ 1112/ 1112/ 111183 111183 1110999 11100731 11100731	ACT - STG -
* * * * * * * * * * * * * * * * * * *	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PP PP PP PP PP PP PP PP PP PP PP PP PP	MATELA 1001-500 76.61 84.34 87.20 85.10 85.10 57.51 50.52
447400000000000000000000000000000000000	100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		e e
717- 717- 717- 717- 717- 717- 717- 717-	20 - 40 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		
	# A # 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	,	
T	4 -	######################################	• 5
23737 23737		1 7 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	913 SEFFE 9564 SEG 91 9764 SEG 91 9764 SEG 91 9964 DISH 9994 DISH 9992 SEG 91 9982 SEG 91 9983 SEG 91 9988 SEG 91 9988 SEG 91 9988 SEG 91
0.00 L 4 L 6 B B B B B B B B B B B B B B B B B B	0.5 F O O O O O O O O O O O O O O O O O O	## W##################################	
# # # # # # # # # # # # # # # # # # #	0.055 0.0155 0.0155 0.0155 0.0155 0.0260 0.0260	88 1 2 4 5 5 6 6 8 8 1 9 6 6 8 8 1 9 9 6 6 8 8 1 9 9 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	10085- 70107- 70108- 70
24 24 24 24 24 24 24 24 24 24 24 24 24 2	0XE6A- 10430- 10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	04 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
U0000000	7 A A A A A A A A A A A A A A A A A A A	2	2
A MENUNA MANA WANA WANA WANA WANA WANA WANA WA	1 00 7 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
> + + + + + + + + + + + + + + + + + + +	RHOVR-1 29.36 29.36 29.85 30.31 30.31 30.34 30.34 30.34 30.34 30.34	1	1
73 X X X X X X X X X X X X X X X X X X X	######################################	7 T Y S S S S S S S S S S S S S S S S S S	DECCE 10 10 10 10 10 10 10 10 10 10 10 10 10
00000000000000000000000000000000000000	24 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	7	DEGERE 10.00 10.32 10.32 9.34 9.34 10.34 1
	MU U U L L L L L L L L L L L L L L L L L	# # # # # # # # # # # # # # # # # # #	O T T T T T T T T T T T T T T T T T T T
EPS.1-1 15.05.1-1 10.1	2000/46144 2000/46144 2000/46144 2000/46144	2	30000000000000000000000000000000000000
#Span / #Span / #Span / #Span / Span	% Span 5 10 15 15 30 30 70 70 96 96	STATOR	% Span 15 10 15 30 50 50 90 90 95

TABLE 7.6
BLADE ELEMENT AND OVERALL PERFORMANCE
70% of Design Speed

á		;)	•							,	
?	% Span	EPSI-1	EPSI-2	V-1	•	VH-1	VM-2		V8-2			. 1-1	2-4	<u>-</u> 5	0-2	H 1	H 2		
		15.759	15. 156	-	_	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	FINSEC F		T/SEC					FT/SEC	F7/56C			FT/SEC 1	\$1/2EC
	2	13.095	13.135	;	772.5		5.08.5	; 0	488.6	-	7 0 0 2	3828	ţ	593.0	2 2 2 2	9 2 8 3 9	4 2 3 5		
	- 15	10.369					587.7		445.0				6554	651.3	715.0	.7165	.5750	788.3	645.8
	Š.	3.070					578.1		361.2				5739	758.1	780-1	-7996	.6038	8 78.6	6.183
	8 8	-5.040	•				512.8		292.1				. 5219	876.2	8 67 .0	• 8 967	.6813	384.9	7.70 3
	2 8	11.547-1	12.77				5 0 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5		3.242				4791	983.6	953.8	.9815	.7606	7.8.01	860.7
	8	-17-428-1	-14.118		477.1		420.4		225.5				1	2 201	0.000	1.0500		1165 0	1
	8	-17-754-	-15.165				383.0		224.5		• •	3872	3890	110001	1062.3	1.0755	. 8071	1183.4	521,2
							:												
	8 6	INCS				RHOVM - 1	- M ACH &	243-2 6		-		•	2224	***	01-2	10.00		,	
	unde a	DEGREE	-	**	4					, -		101-51	IZ-IOI IZ	SI PERFE	F DEGRE	TERE SER	F 7/5 F C		
	s	**		•				•					68 20			4 -593.4	-122.4	ļ	
	2	-14		~			46.93	.3278					12 98.		12 18.7	18.76 -627.4	-204.7		
	21 22	2.		_				٠.					89 97		14 24-5	7 -661.3	-270-1		
	2 5	1 25											31.		37.8	9 1-758.1	-418.9		
	2 8	4-42					38, 20	27.16.				89.32	32 88.30	96 62.88	7.64 86	48.25 -875.2	70-		
	88	4 . 4												i		2-1063-2	-794.		
	8	4.60	5. 67	6.32	80.08	8 30.41	n	.2821	1443	.0249	1-1910		81 69.08			62.35-1083.1	-815.0		
	8	1.70					5							•	ř	5-1104-1-837-8-	-837.8	:	
							1												
					10/10 1 1 1 1 1	PO/PO	EFF-40	1 1 1 1 1	* #C1/A1										
							- - - - -	- 1 H	SOFT										
					1.0859	1.287	9 87.32	87.72	30.49										
	<u>\$</u>																		
Š	Span	EPSI-1	EPSI-2	<u>-1</u>	4- 5	VH-1		.1-6				1-1	H-2			_	PT 2./	1127	
		DEGYEE	DEGR EE	FT/SEC	FT/SEC	•	FT/SEC. FT	VSEC F1	õ	ఠ						•		111	
	•	14.059	4.548	838.1	3.28.5		826.4	31.9					7349		-	٠.	•	1	
	2:	12.300		826.1	826.1		824.1	73.1					917			∴ .		5 0	
	2 8	10.861		.93.8	801		799.66	53.1					71 87					9707	
	2 8	7.149		663.8	675.3		673.7	1 1 1 1 1 1 1					50.45				1	6.80	
	8	-1.514		630.0	622.8		671.2 2	8.55					5945		•	-		6 : 40 1	
	92	-4-129		615.6	570.9	571.3	569.6 2	28.2					5059		-	-1	- 1	07.38	
	 8 %	-5.125	464	594.4	550.8	547.7	549.4 2	231.0	-38.4	23.0	0 9	.5274	4867				1.1657	1.07:6	
	?					1	•			,					-	•			
	, C	200	2	2	101	1, 10,00	C - M MOTI O	0	G - 4 3	-	013/	- 6 6 6	۰				SEFF-A	4-FFE	
	nd o	DEGREE	DEGEE	DEGREE	338 830	•			TOTAL		, II	STATC-ST	. 15				Tor-ST		-
	\$	-2.70	.22	12.51	# 3 . F.9		59.28	.1824	.1457		9546	9-462.D	-				77.46		
	2 :	-6.19	-3.26	11.52	39.14		60 • 32	.1561	.1053		9690		•		3		88.74		
	2 8	-7-19	-4.25	10.92	37.21	2006	59.01	1450	0.0870	-0214	9756	200 state 32/6 .	on C				88.18	9. 4	i
	2 2	1 0 1	7.5	12.04	00.00		14.00	1747	01330		200	177.5	, ,		No.		86.18		
	2	-12.80	-9-57	13.45	26.87		16.60	1501	.0563		983	2-135-6					80.10	1	ı
	82	-13.60	-10.28	15.89	25.91		47.28	.2215	.1283		.976	5 11.3	•				00.99		
٠	8 8	-12.65	-9-32	17.40	26.95	£0.5	95.04	-2320	.1112	.0394	386.	25.4	٠,		•		. 59.33	6.25	
	<u></u>	-12-04	-8-6-7	18-68	2.1	-,	38.09	•2609	•1 388	•	. 978	2005					70070	: -	
		_	9	0	-	0	04.777	9 (3)			٠.								
			INCET	INLET	INLET	INLET	IN ET	INLET		•									
				1 15.15	1.0859	1.25.51		8											
	_			4 300 4		7		,											

TABLE 8.1 BLADE ELEMENT AND OVERALL PERFORMANCE 90% of Design Speed

-			
	V**Z 508:7 508:7 568:7 625:5 625:6 730:6 803:5 860:4		
	V*+1 67/5EC 876-9 921-8 951-8 1077-9 1336-1 1447-5 1477-6		11.2030 11.2030 12.1034 12.1034 12.1031 12.2031 12.2031 12.2360 12.2360 12.2360 12.2360 13.236
,	2 -4399 -5421 -5629 -6225 -7086 -7086	7	48 48 58 58 58 58
	M*-1 H .0009 .0777 .0777 .0177 1.1111 1.2213 1.3013 1.3215 1.3420	B*-2 VB*-1 DEERE FF/SEC 1 10.21 -74%.2 17.23 -42%.2 19.42 -95%.5 19.42 -125%.5 54.98-1258.6 50.75-1358.9 63.25-1390.2	### ### ### ### ### ### ### ### ### ##
	0-2 645.7 645.7 873.0 970.3 970.3 1091.7 1201.0 1201.0 1310.3	81. 581. 581. 58.01. 58.01. 66.02. 70.83. 70.83. 70.83. 58.01. 70.83. 70.83. 70.83.	· · · · · · · · · · · · · · · · · · ·
	U-1 7475EC 790.0 832.7 954.5 1103.3 1138.6 1338.6 1338.9 1358.7	4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.	
	#-2 7792 7693 7593 6518 6518 5919 5919 5673	2001 2001 2001 2001 2001 2001	## 12
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		P12/ P11 P11 P12 P13 P18 P18 P18 P18 P18 P18 P18 P18 P18 P18	######################################
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	71/5EC F 889.9 881.5 881.5 732.1 732.1 716.2 716.2 698.5	DECREE 41-19 41-19 36-41 22-75 36-41 17-10 11-09 11-45 7-60 7-60 7-60 7-60 7-60 7-60	V-2 V-2 V-2 V-2 V-2 V-2 V-2 V-2
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	EPSI-1 EPSI 15-971.15. 13-522 13.1 10-870 11. 10-870 11. 10-870 11. 11-228 11. 11-228 11. 11-228 11. 11-338-12.	TMCS TREEFE 2.858 2.958 4.14 4.24 5.58 6.54 6.54 6.54 6.54 6.54	DEPKI 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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TABLE 8.2	AND OVERALL PERFORMANCE
	BLADE ELEMENT AND

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TABLE 8.3 BLADE ELEMENT AND OVERALL PERFORMANCE

90% of Design Speed	FSI-2 V-I V-2 VHTI VR-2 VB-I VB-2 BFI B-2 H-I H-2 U-L U-Z ML-1 ML-2 LISIE FISEC FISE	DECKEE D	DEGREE F/SEC	MCAR DEV TURN RHOVM-1 RHOVM-2 D-FAC OMEGA-B LOSS-P PT2/ SEFF-P DEGREE D
	EPS711 [EPS712] [INSTITUTE OF COLUMN [INSTITUTE OF COlumn [INSTITUTE OF	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		######################################

TABLE 8.4
BLADE ELEMENT AND OVERALL PERFORMANCE
90% of Design Speed

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		DEGREE	DEGREE	FT/SEC.		1/5EC F	•	اد ان ان	ă	REL 05	*		•	•		•	-	-	13.5
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	, 9	200	17.276				9,449		22.2		• •	•		•		•			
1, 2, 2, 1, 1, 2, 2, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	2 2	10.538	11.220	559.3	975.7	7	657.2	, 0	78.7			• •			_	•	_		9, 8
See Fig. 1 1 1 1 1 1 1 1 1 1	8	3.342	. 557	5.83.	786.2	83.2	611.7		93.8		•			_	_	•	_	۰.	45.2
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\$ -17.00 -1.	88	-16.029	17.333	573.6	656.6	73.6	537.7		76.8		•	•	1365	_	_	•	-	0.	15.8
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No. No.	8	-17.549	15,000	565.4	5.5	*	453,0		97,2		•	•	_	_	_	•	- 25	•	1.
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10 10 10 10 10 10 10 10	S		5.72		38.86		51.71	0444		.0273					5.86 -7	92.1 -1	78.6		
1		94	. 5.97	15.57	33.81		56,46	4227		.0038					9- 1	0.50			
State Stat	S1 :	=		14.56	29.24		26,10	.4207		00000					7,22 .8		34.0		
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99 9 9 9 9 9 0 0 0 0 0 0 0 0 0 0 0 0 0	2 :	3,73	4.95	• 5 •	٠	38,31	46,53	.3615		,0226	. 528				61 - o t .	5.5			
Sun Sun	8 8	3.69	90.	.0.9	•	38.10	15.0	3773		.0291					2.00.13		,,,,,		
Sign DEGREE DEGREE FISSE TIVET INLET REFERENCES BELL BG-2 1.1621 1.5776 86.35 87.07 37.90 1.1621 1.5776 86.35 87.07 37.90 1.1621 1.5776 86.35 87.07 37.90 1.1621 1.5776 86.35 87.07 37.90 1.1621 1.5776 86.35 87.07 37.90 1.1621 1.5776 86.35 87.07 37.90 1.1621 1.5776 86.35 87.07 37.90 1.1621 1.5776 86.35 87.07 37.90 1.1621 1.5776 86.35 87.00 1.1621 1.5776 86.30 1.57	ç	, 0,	*	٥,٠	3.42	37.91	38.51	. 387		.0324			50.	ç		7.5	•		!
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1, 10.2 1, 1						:			5017										
Span DGGREE PTSEC FTSEC					1.1621	547	88		37,90										
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12.160 7.062 1.064 722.3 893.7 603.0 -46.4 92.6 -5.0 8559 7.734 1.6403 1.2160 72.3 893.7 762.7 893.0 -46.4 972.3 893.7 762.7 893.0 -46.4 972.3 893.1 762.7 10.507 1.2160 1			DE GR	•	i.	FT/SEC			5	GREE DE	أغما					P		=	
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-5.385 "440 765,7 65.0 656.4 649.5 394.7 -44.4 31.1 -3.9 6627 5565 14136 14136 14520 14520 14136 14520 14520 14520 14520 14520 14520 14520 14520 14520 14520 15520 14520 1	82	707			•	. ~											• •		
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-2.81 .12 [2.50] 41.58 61.75 61.75 61.75 61.75 6.0241 .9556 41.91 99.52 99.52 -3.42 -4.8 95.6 91.91 99.52 99	ء د	-		15.7				•		•	. 7536	45.71	٠.,			-		84.7	
-3,42	2 5	-2.8	•	5 . 5				•		٠	. 9567	46.50				•		91.16	
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-4.51 4.50 1.50 34.00 55.01 52.00 5.10 5.10 5.10 5.10 5.10 5.10 5.10 5	88		;					•		•	7.0.	72.17	٠	٠		•		63.53	
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TABLE 8.5
BLADE ELEMENT AND OVERALL PERFORMANCE 90% of Design Speed

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% Span	EPSI-1	I EPSI-Z E DEGREE F	V=1 FT/SEC	V=2 FT/5EC	VM-1	VN-2.	V8+1 .	VB-2	8 = 1	8-2		H+2	1-0.1	U-2	N. sea	H-2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7007
s ;	15,808	16.432	5 45 .5		545.5	•		677.2	3 0 ·		, 5005	•	760.5	860.7	.858B	.5916	9,35.9	675.4
2 5	13.183 13.	13.290	557,3		557,3	689.1		623.8		42.0	6115		. 904.	888.6	.8987	.6 *87	978.3	738.2
S 5	10.522	11.282	568.6		568.6	6.999		582.9		0.14	5229		4.7.4	410.4	9346	6532	1020.4	7.15.4
₹ 5	5-4-5	- 69.6	593.5		543.5	632.7		489.9		37.7	1 2 + 5		971.6	6.666	1.0496	.7088	1138.5	812.6
5 5	909.	-1.062	606		606.3	592.7		429.1		35.9	9655		122.9	11111	1.1780	.7835	1276.2	913.6
2 %	A 7		544.2		599.2	572.7		371.4		32.8	. 5527	_	260.7	1222.4	1.2875	9698	1395.8	1025.8
8 8	10.214	12,51	563,6		583,6	547.4		349.3		32.0	. 5375	-	362.6	1305.9	1,3652	.9505	1482.3	1102.1
? 8	-17.205	-13.953	579.1		579.1	504.5		352.8		34.5	5331	_	368.2	1333.6	1.3846	. 9463	1.504.1	1103.0
£ -	-17.660	-15.097	575.2		575.2	457.7		352.9		37.3	5293	4935 1	415.0	1361.5	1,4055	9457	1527.4	1107.6
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% Span	SURI	I OZ		TURN	RIOVH	T > O I X	2 D-FAC	OME GA-	-		1000				42			
•	REE	DEGREE	DEGRE	DEGREG				TOTAL			101		~		FT/SEC	FIVSEC		
~	. 22	5.21	_	38.54		52.98	•				1 91.		•		4760.5	-183.6		
₽		5,46	4.0	34.20		57,32	•				3 97				1.804.1	. 2 A H . B		
-2	. 68	5.40	13.8	29.43		55.74									7 - 8 - 7			
33	6	4.56		19.61		53.65	•								4-126- 4			
20	7.06	4.72	9.9	12.71		50.43					7 88				8-1-2	2 84		
02	2.0	2.01		8.85		06.00					15 97							
. 82	3,35	4.58		7.02		4	•								4 1 2 6 0 6 7			
8	3.57	4		1			•				•				1 204 .	000		
95	3.67	4.57	6.38	2.57	36.36	36.21	35.45	1933	9000	1.4193	3 69,74	74 68,24	67,88		05.30-1415.0-	1-1006.6		
						•												:
				10,10	P0/P0	EFF-AD		4/13										
				INLET	ÄLE	-	INCETLE	LBM/SEC										
						<u>,</u>		505										
				995101	1.5714	•		38,38										
				•														
STATOR																		
	EPS1+1	EPS1-2	-			VH-2	1.01		B•1	8-2	÷	7-1			- :	P12/	771	
•	OLGREE	0 6 6 8	FT/SEC	•	F1/5EC F	-		ä	GHEE DE	GREE					_		Ξ	
^ :	7.0.5	.n	1003		758.9					•	•	6089,			-	. 6065	.1868	
2 5	14.331		5	_	789.3 1					•	•	1006			~		1766	
2 5	10.817	•	7.96.7		769.4					•	•	4769			-		1707	
Q 5	6.737	~	882.0		738.3					•	•	. 6031	•		-		. 1569	
2 5	2.0.6	7 . 7	826.4		707.1					•	٠	7454		:	-	ij	4 15 25.	
o v	-1.733	•	745.6		701.8					•	٠	.6924			-		. 1453	
8 8	100	•			0.007				27.0	•	6874	6616			<u>.</u>	* 187	80.	
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?	7	•			0.00					•	•	6273			-		7 .	
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S S Date	2000	06.50	DE GDFF	•	ĸ	Ė	2 D=4 VC		10055-1		1 1 1 1 1					TOT-STG		2
s	-1.26		12.51	•	4	71.78		969	.0472							77.61		
10	-3.65	•	11.52		. •	6B * 4		1169	0298		343.1	•				96.40		
21	-3,83	•	10.92		•	73.72		9680.	-0234		7 196.5					66.97		_
8	-5,23	1 2.	11.25		, ,,,	40.85		107	.0302		7 225)					80.48		
S :	-5.52	-2.38	12.03	35.15		64.38	151	.1322	*0 *0		.9413 305.50	0				79.60	80.69	
₹ 8	-7.56	*	13.45		un	59.70		.2061	1 8 9 0 •		0-921.3	5				73.41		_
8 8	-6.47		15,89		u	54.76		,2339	4.0834		8-215-3	•				66.82		_
3 8	60 /	•	17.40		. ,	55.63		. 2019	•0716		8-300.7	2				62.94		_
2		13.21	80°.		un .	52.43		• 2053	•0739		8-237.	•				57.85		_
		~	#CORR	10/10	P0/P0	EFF-AD	E F F * P											
		RPH	INLET BM/SEC	_	INLET	INLET	_						•					
		٠.	170.16	1.1564	1.4967	77.95	•											
				•														

TABLE 8.6 BLADE ELEMENT AND OVERALL PERFORMANCE 90% of Design Speed

2000 2000 2000 2000 2000 2000 2000 200				
V*-2 C FT/SEC 1 755.3 1 755.3 5 814.2 5 908.8 8 1100.8 6 1101.7		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	FEFF-P TOT-STG 78.71 90.59 90.59 90.59 86.77 68.05 68.02 63.03	
V*-1 F7/SEC 937.6 980.1 1022.6 1140.5 1238.1 1506.6	Viet in a manage	772/ 711 1.1894 1.1741 1.1591 1.1551 1.1550 1.1557	a-e-	
-2 5938 6684 6622 7101 7882 9474 9419		PT2/ PT12/ PT12/ 1.66132/ 1.66339/ 1.66830/ 1.66830/ 1.68820/ 1.36830/ 1.36830/ 1.36830/ 1.36830/ 1.36830/ 1.36830/ 1.36830/ 1.36830/	######################################	
#-1 # # # # # # # # # # # # # # # # # #	0.42 V0.1 15.04 -762.1 25.70 -869.8 26.70 -899.8 3.857 -913.5 9.85.93-1263.3 59.33-136.5 59.33-136.5 50.05-1410.1	** ⁻ ਜੱਜੋਂ ਜੋ ਜੋ ਜੋ ਜੋ ਜੋ ਜੋ ਜ	·	
	7	and the second s		
0-2 FT/STC FT/STC B62.6 B90.3 1102.0 11113.5 11308.7 11308.1	13.53 13.53		. *	
U-1 762.1 762.1 805.8 849.4 1125.3 1355.5 1391.1	0.00 0.00			
• • • • • • • • • • • • • • • • • • • •	440 11 10 10 10 10 10 10 10 10 10 10 10 10	5 54 65 65 65 65 65 65 65 65 65 65 65 65 65		
88231 97384 77384 77384 55325 55325 65325 65353	16 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		######################################	
#-1 -5012 -5237 -5477 -5477 -5536 -5370 -5370 -5370 -5370 -538	P12/ P12/ *7595 *7595 *6195 *6192 *6192 *94913 *94913 *94913 *94913 *94913	######################################	P72/ \$EFF-B7 9228***********************************	
8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	. Desemble	100 100 100 100 100 100 100 100 100 100	•	
	1005-P	8-1 169EE D 41-3-3 36-1 35-1 30-8 27-9 27-9 28-6	1055-P 10154- 10154- 10154- 10151- 10	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00FC6A-8 70744 1382 1382 1382 10857 10958 1721 1721 1721 17214 1721 1721 1721 172	ä !	0MEGA-B 104 A4. 1902 1210 1210 1241 1890 2186 2198	
V8-2 FT/SEC 612-3 612-3 517-7 93-2 454-2 454-3 351-3 352-3	8 ET 6655	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	# 6 00 00 00 00 00 00 00 00 00 00 00 00 0	8.
74.	I SHEET WHINN WAR	71/06 60 00 60 00	·	63 78
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VM-1 17/SEC 5585.2 5586.2 5586.2 5586.3 5588.3 5588.3 5588.3 5578.5 5578.5	HOUN-1 35.95 37.55 39.27 39.27 39.49 38.75 38.35 38.35 38.35 1NLET	VM-1 71/550 71/50 804.7 746.9 746.9 704.7 704.7 704.7 704.7 704.7	59.19 63.72 63.72 61.57 59.42 59.42 56.15 56.15 56.15 99.90 19.70	1.4975
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BLADE ELEMENT AND OVERALE PERFORMANCE 100% of Design Speed 100% of Design Speed

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% Span	DEGREE DE	_		_	•	T/SEC F	1/SEC F	1/SEC 0E	GREE DE	GRE	•	•	FT/8EC	FT/SEC		,	T/SEC F	1/SEC
\$	15.915 18		562.9			647.9		9.608	•			.8357	850,3	462.4	.9372	4869	019.7	569.1
10	3.39		575.5			6.804	•	744.0	•			, 6254	0.668	993.6	. 9822	. 5649	067.4	, , ,
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23	3.549		615.6			539.5	0	633.8				, 7059	1086.3	111/01			0.017	
20			5.000			5.00	-					4 6 6 6		1272	1.3004			
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88						- 0	•	7 0 0 0			000	77.00			5.183	9.176	466.4	998
3 S	17.331-14	14.848	601.9	748.1	60109	427.4	•		•	54.8	. 5553	+609	1582.1	1522,3	1.5618	. 8177	1692.7	1003.8
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	91.1	45.	2.6	35.06									44 57		6 -899.0	-249.5		
	1.37	7 . 45	14.70	30.65				•	-		_	_	07 58.6		4 -947.7	-333.4		
30		6.45	12.01	18.40		Va .							29 60		0-1086.3	1.484		
S :			7 . 15	13.84									85 63		2 : 652 ! = 2	7.070-		
0,6			5.62	5.5											0 - 1 4 O 4 . 5	7 4 4 4 4		
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S 66		5.83	7.55	9.4	39.63	95.14	5405					16 71.63	69 69		8-1582.1	-908.3		
				10/10	04/04	EFF-AD		#C1/A1										
				INLET	INLET	INLET	INLET	LBM/SEC										
				1.2512	1.9928	86.57		39.48										
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STATOR		_										:			,			
uado «	DEGREE DE	EGREE F	F1/SEC F	FT/SEC -F	T/SEC	FT/SEC FT		FT/SEC DE	GREE DE	GREE.	-	7-1			_) - L	711	
~ ;	3.730	_		733.1		731.9			2.15	3.2	8678	16091	٠.		_		.2490	
2 %						713.1 7					0198	.5956	-		_		.2344	
2 8	215					688.7					.8467	.5784			<u>.</u>		1.2269	
: S						0.000					7513	53.3	•		<u>.</u>		6 7 7 7	
0,	. 9 20					637.2 E					7	2016	·		-		26.75	
88		_				635.1 6		٠			7297	5179			• -		27.94	
8 8	5.387					622.8 6					7228	5040	,				2917	
ŝ	*					9 **009					7129	.4831			-		.2996	
8	2	X	,	, 2011	3	2		0.45.04.0		, ,						4. F. F. F. A.	SEFF-P.	
7	DEGREE DE	DEGHEE D	EGREE	DEGRE		 		TOTAL	TOTAL		STATC	-81				TOT-STG	ſΗ	
•		1.65	19.62	40.01	56.29	73.28	4505	.1219	.0303	952	9 79					84.70	86.05	
0	20.5	7.96	13.29	48.59	62.63	72.50	4696	.1598	.0408	.938	B 73.	06				89.47	90.39	
<u>\$</u>	3.17		9.12	49.39	65.65	70.56	4872	.1752	.0457	*66.	4 71.	7.3				91,19	91.95	,
≥ 5	9	9,0	9.6	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	57.64	66.33	4912	1060	.0253	. 97		•				87.74	HB.77	
5 6		2 .	10.21			9.00	929	0001	•030	. 06.		.				93.4	70.70	
88	8.59	10.0	15.58	0 7	58.57	40.64	5.36.5	241	. 040	0 0		_	•			79.92	81.63	
	0.21	55.0	0.40	48.82	60.09	61.29		1889	200	7	. 97					200	7	
	11.28	. 65	21.83	49.00	53.86	50.50	.5773	.2129	.0768	938	05.49	. 0				64.39	67.29	
	202			10/10	P0/P0	EFF-AD	EFF-P											
	¥ .	NLET	INLET	INCET	INLET	INLET	INLET											
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TABLE 9.3 BLADE ELEMENT AND OVERALL PERFORMANCE

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	100 100 100 100 100 100 100 100 100 100	122/ 102501 1025	######################################
M ** 1	22.26 - 943.6 22.26 - 943.6 22.26 - 943.6 22.26 - 943.6 22.26 - 943.6 22.26 - 943.6 22.26 - 943.6 23.26 - 943.6 24.28 - 11.1403.4 26.38 - 18.1403.4 26.38 -		
U-1 0-2 0-4,6 0-4,			
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#S.8.	o.*	STATOR *S	ir.

TABLE 9.4	BLADE ELEMENT AND OVERALL PERFORMANCE	

		•			BLADE	DE EI	ELEMENT A	NT AND 100% of		OVERALL PERFORMANCE Design Speed	ALL PI Speed	ERFC	RMA	NCE				
ROTOR					•	•			`.	•				-				7.0
% Span	DEGREE DEGR	, 4	/=! /S£C	V=2 FT/SEC F	7/5EC #	7/5EC	_	1/5EC DE	GREE DE	GREE		_	1/SEC F	77/5EC			T/SEC !	FT/5EC
•	15.845	15,462	85.2			598.3	_		ć		•			955.1	4	525	0.026.9	622.
2 2	13.289	13,328				642.8		7.7	•		5522	6386		9.0	1.0365	7	122.2	750.5
- R	3.455	5.605	9.1.			585.8		63.7			•			5.601	1.1624	.000	254.5	774.0
S	-4.356	-1.046	57.1			\$75.4	_	6.1			•	_		233.0	1.3075	.7347	7.00.1	
2 3	-11.255	7.488	80.6			***		9.4			•				1.4308			20.00
8 8	10.070	13.744	27.8			478.7					• •			7	1.5389	. 7 2 8		6.6901
88	-17.521-	14.962	623.4			130.2	_	1.5			•	_		9:015	1.5422			000
	, ,	- 2			3	9		4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7						-	9.	```	_	
% Span	20000			2 2 2 2 2			1	TOTAL				101	016868	DEGRE	11/SEC	FT/SEC		
8	-	9.15		39.13	38.86	52,92	.5742	.1387					55.1	50.61	-843.9	-172.7		
2	•0		5.40	34.35	39.49	58.26	5234	.0485				9.96	55.4	21.61	-892.2	-754.4		
Z 5	1	6.2		29.77	0.10	61.70	4847	*10.				0.00		56.92	2 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	1505-		
3 5		77.5		18.34			400	7				62.6	62.24	10.5	1246.0	5 -		
8 2	99.0			0.37		21.5	*	1254				. 65.2	11.69	56.76	1-1390.9	-837.9		
8	3.81	5.03		*6.9	00.14	8.9	8995	.1812				78.3		4 60.23	1-1512.0	-922.9		
8 1	3.96	5.03	-,	5.15	40.78	44.89	. 4823	.2219	.0379	1.0310	75.77	73.67	67.79	62.65	62.65-1540.4			
95	21.	20.0		3.0	40.54	*0.47	804.	. 2537				•		65.2	1.0/61-			
				10/10 18/61	PO/PO	FFF-AU INLET	1 F F - P	BA/SEC										
						-												
				1 - 2 30#	1.8984		•											
STATOR										,								
Spen	EPS1=1	EPS1-2		~ .	V#-1	2-17			3.1		:	~-)	
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01	11.891	-	1019	778.8	733.2	777.9					•	295			-		1.2282	
21	10.432	3.823	446.7	757.7	744.3	753.4					•	1393					1.2175	
8 8	6.725	2.916	• • • •	705.1	676.8	701.0					•				-		2301	
2 2	10.763	733		658.5		454.7					•	1487			-		1.2256	
88	-4.349	140	-	634.6	654.3	134.1					•	6429			-		1.2450	
8 X	-5.319	. 576	1.1.6	617.9 583.8	634.3	617.2	. 60.00	- 54° 6	41.2	7.7.	. 6404.	4757				.7292	1.2642	
	-				:										•			,
d	S)¥I	_	DEV	TURN RH	RHOVA	RHOVH-2	P D-FAC	ONE GA-B	2	P14/						PEEFF-A	AETET-P	c
,		DEGHEE	DEGREE	DEGREE		,					-					97.50		
. 5			12.75	4 4 4	44.25	76.17			97.60							88.75		_
. 2				47.30		73.52			0000							41.07		~ -
8	2 40			47.54	60.72	96			4.10.					•				
8 8			7.11		59.83	9 1 1 8 9			7610							82.49		
88	9	-	4.87	0 * * *	58.41	0.0		1109	.0386	9480	78.44					73.35		• •
8 8	19.5		79.0	40.0	55.75	20.15			***			• •						
\$:	_	77.0		, ,										-			
		NCONR	#CORR	10/10	P0/P0	EFF-AD												
		_	INLET ON/SEC	INLET	INLET	INLET	INLET											
			_	1.2308	1.0423	92.54												
	_				•													

TABLE 9.5 BLADE ELEMENT AND OVERALL PERFORMANCE 100% of Design Speed

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w w	? :	•	_	•	•		DEGREE D		014	_	FT/SEC	FT/5EC	. 9542		F7/SEC -	77/5EC
	2					711.5	? ?		.5436	06.00	696.7	991.0	1.0017	-		754.7
•	~ ;					651.3	•		5771		J. 180	1022.0	1.0475		1132.7	7.4
	2					9	•				252.4	239.2	1.3203			642.3
~	2					5.95				-	0.40	363.3	907		552.2	1068.2
_	5					467.5			2005	_	1519.7	1486.4	1.5243		1648.0	1129.1
	7					4.7.4	•		9995	_	1548.2	1487.4	1,5481		1472.5	1127.3
us.	2					471.9	•		. 5 6 20	_	1.674.1	9.0191	1.6719		1,990.	1135.2
	ž				•	•				;						
•	30	٠	Š	HADER T-E	H-2 D-FA					-P 5EFF	•	20.80			~	
•		•					_	-		100	•	7.5		204.1		
					•					20 94		23.2	7 -896.7	-299.8		
	ċ							_		24 96.		20.3	2 -945.3	1 -370.7		
	ċ							_		74 92.		0.01	4-1083.5	5 -535.1		
	;				•			_		13 68.2		5 49 5	1-1252.4	1 -706.2		
					•			-		69 63.5		0.95 0	4-1406.0	-407.9		
	:				•			-		76.7		2 61.7		0.666		
è	:	0	3.34 40.49	42.73	73 .4272	\$ 22.0	*****		95.17	15.74 45	200/0 19	7		0 * 10 1 = 2 : 0 F 0 1 = 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +		-
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CGREE FT	₹	EC FT/SEC	C FT/SEC	. FT/SEC	F 7/5EC	FT/SEC D	EGREE	DEGREE		•				=	=	
_	5		4 755.9	987.5		•	*.	:	9916	.7862			-	. 8785	. 2319	
	2		5 792.2	673.4		-63.7	. O	6.5		965.			-	5586.	.2179	
_	:			291.02			~ .	•		/18/			→ •		2132	
								•		000				****	/ /07	
						47.5				245						
	20		6 475.7	636.5		-84.2	7			5337			•	6356	.2153	
	102		2 647.5	413.2		-33.8	36.6			. 5100			-	. 6004.	. 2242	
	Ī		. 424.7	671.2		:	30.0	-1.7	:	.4710			-	. 5482	1062.	
	5		076	9	10.0	OMEGA	_			•				SEFF-A		
	3	_		•		TOTA			111	- 51				TOT-STC	TOT-STG	
•	9	•								. ~				45.02		
	12.00				•				7.					91.07	41.62	
										17				17.14	92.39	_
~		43.31	31 43.51	73.23	13.385	2 .0447	0125		86.76						40.22	
	:								96	91				46.33	,	
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	3				•				. 78.					70.13	72.09	
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	-				•				73.0	~				84.40	42.02	
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TABLE 9.6
BLADE ELEMENT AND OVERALL PERFORMANCE

TABLE 9.7 BLADE ELEMENT AND OVERALL PERFORMANCE 100% of Design Speed

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